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The Hydrogeology of the Nyamazura Area.

by

Jeffrey Davies

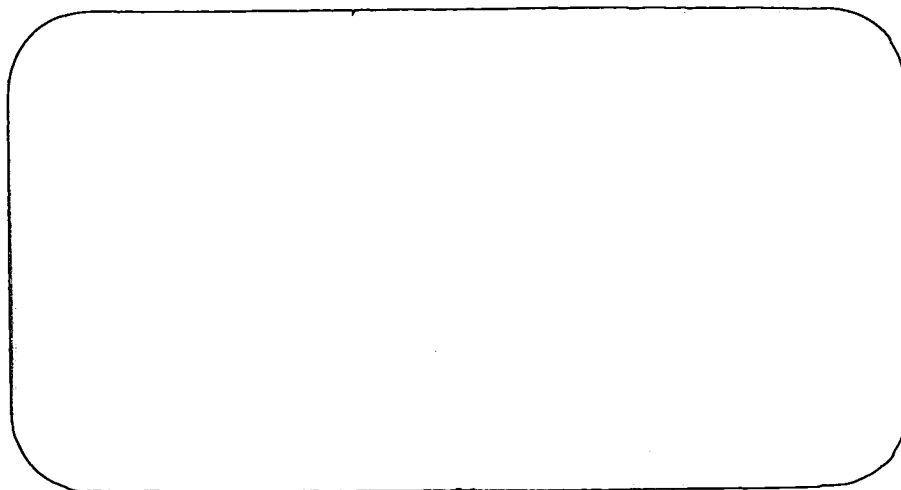


Natural Environment Research Council  
British Geological Survey

EPW file  
310

# HYDROGEOLOGY

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## THE HYDROGEOLOGY OF THE NYAMAZURA AREA

### 1. INTRODUCTION

#### 1.1 Background.

The development of the Nyamazura Intensive Resettlement area is being jointly funded by the Government of Zimbabwe and the British Government. The British funded Primary Water Supply Unit of the Ministry of Water Resource and Development were required to undertake an exercise of borehole drilling, cleaning and equipping to supply good quality domestic water supplies to a series of twelve villages located within the scheme area. This work was undertaken during July-September 1984, during which time a series of 13 holes were drilled (9 successfully) and 3 holes were cleaned out. All holes were equipped with hand operated Bush Pumps of local design. While undertaking the above work the opportunity was taken to make a fairly detailed assessment of the hydrogeological potential of the Basement Aquifer in the area (see Fig. 1).

#### 1.2 Location.

The Nyamazura area is located some 40 kilometres west of Mutare in the Manicaland Province of Zimbabwe. The area encompasses some 10,830 hectares of farmland located north of Odzi primarily between the Odzi and Chingwadow rivers.

#### 1.3 Topography.

The topography of the area is of gently undulating aspect with prominent hills to the west (Chenyamatsini 1320 metres), the north (south of Game Valley 1213 metres) and the north east (in Osbourne up to 1250 metres). The drainage pattern is rectilinear in form being developed upon primary structural lineations that trend NW-SE, NE-SW and N-S. The main rivers are the Chingwadow, Inyamazura and Odzi. Only the latter was flowing after 3 years of drought in September 1984.

#### 1.4 Climate.

During the last 50 years annual precipitation has varied between a maximum of 1300 mm and a minimum of 370 mm (see Fig. 2) (average of 700 mm p.a.). During the period of 1982-84 the area has experienced drought conditions with annual rainfall of 550 mm or less. The rainy season usually lasts from 3-5 November until 28th March. Evapotranspiration rates are not known.

#### 1.5 Vegetation.

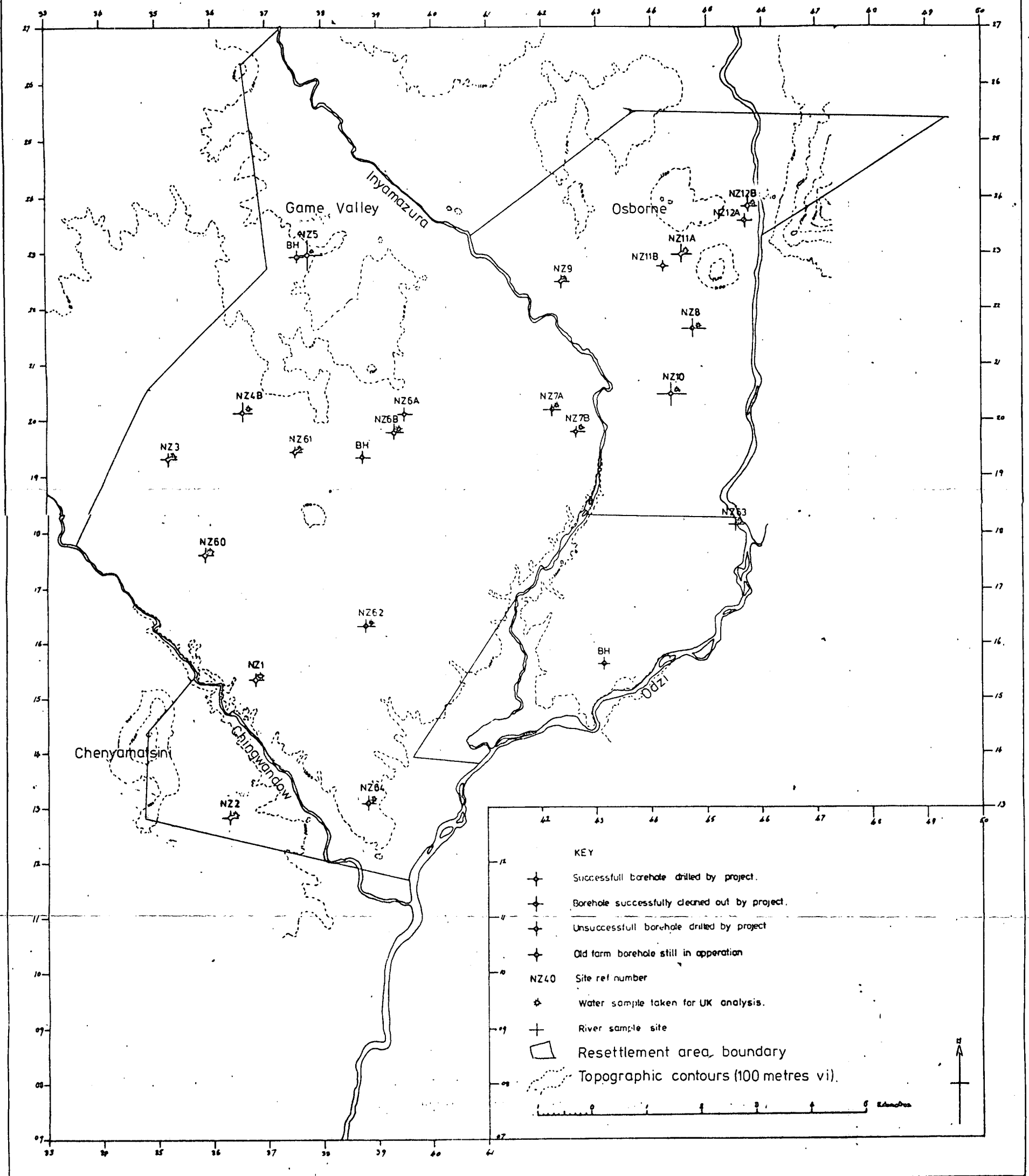
The natural vegetation of bush scrub has been replaced over much of the area by open grassland as a result of farming activities, primarily cattle ranching and the cultivation of tobacco and maize.

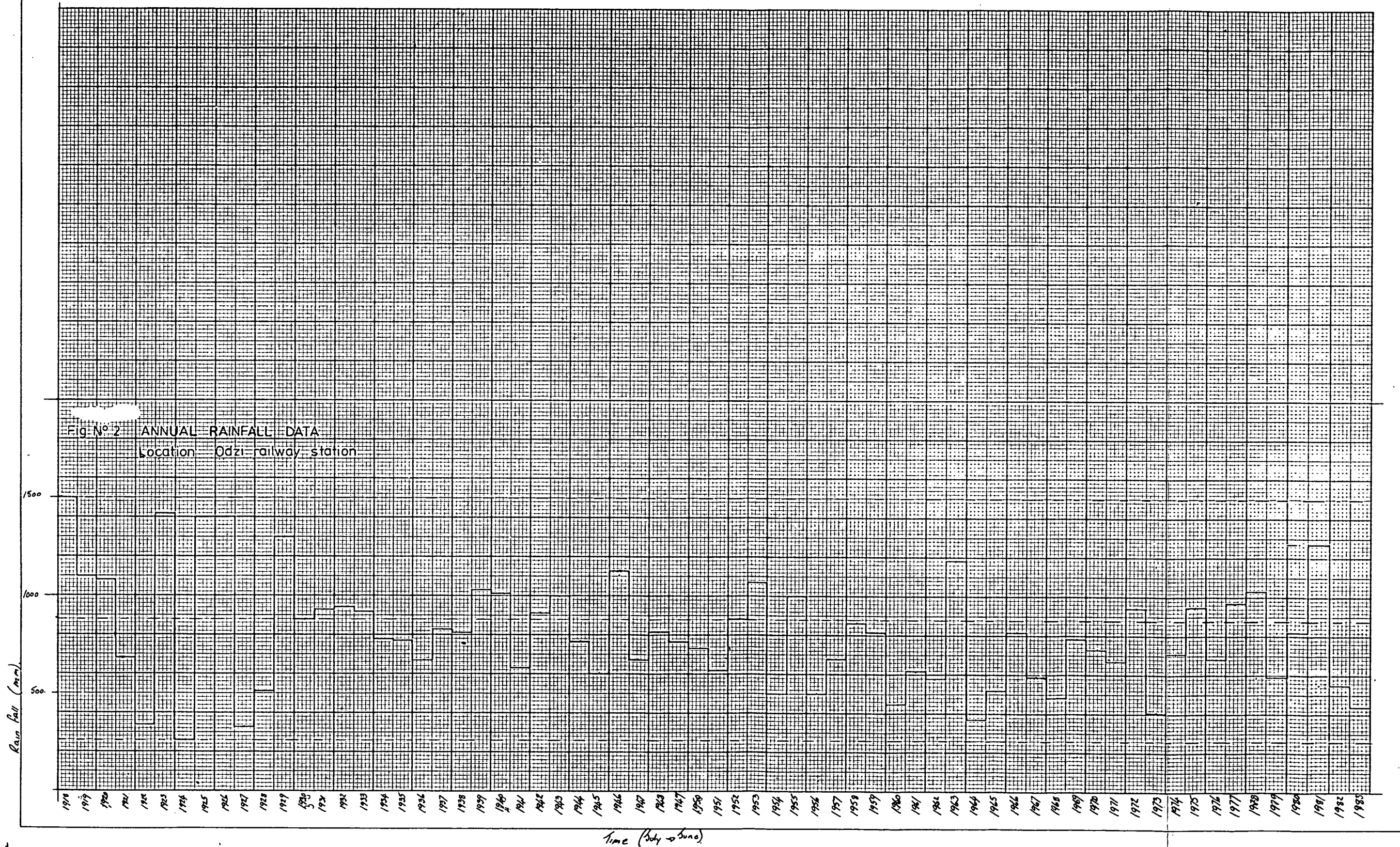
#### 1.6 Population and Settlement.

The resettlement area encompasses a series of former commercial farms, now vacated. The proposed pattern of settlement within the Nyamazura area is described in detail within a report prepared by Agritex (June 1981). The PWSU were primarily concerned with the supply of domestic water to a series of 12 peripheral villages in which 400 plus families have been settled.

# INYAMAZURA RESETTLEMENT SCHEME

Fig N° 1 BOREHOLE LOCATION MAP





## 1.7 Aims of the Project.

The primary aim of the project is the provision of a source of good quality domestic water within 0.5 kilometres of each village at as low a cost as possible. During the project, opportunity was taken to conduct a fairly detailed hydrogeological investigation of the area that included the collection of sludge samples from each newly drilled hole, the test pumping of new and cleaned out holes and obtaining water samples for chemical analysis from new, cleaned out and old boreholes and as and when access permitted. It is hoped that the report produced will provide an additional insight into the occurrence of groundwater in Weathered Basement strata.

## 2. GEOLOGY

### 2.1 Introduction.

No detailed geological map of the Nyamazura Resettlement scheme exists. To obtain an understanding of the geology of the area two sources were consulted, i.e. the National Geological Map of Zimbabwe that provides an incomplete description of the geology of the area, and Swift (1972) which describes in detail the geology of the Odzi Gold Belt that lies adjacent to the southern margin of the area.

Additional data especially of a structural nature were derived from a study of topographic maps and aerial photography to locate linear fault/joint zones. During the project period geophysical surveys using EM and Wenner type resistivity arrays were used during the location of drill sites. The boreholes drilled yielded detailed geological data. Unfortunately no data whatsoever were forthcoming from the pre-project boreholes.

Details of the data sources used are presented in Appendix I.

Of prime interest to the project were a knowledge of rock types, depths of weathering and occurrence and nature of linear fault/joint fractures.

### 2.2 Pre-cambrian Basement Strata.

For the purposes of this report the Basement Precambrian strata have been divided into two (see Fig. 3):-

- (1) Granitic gneisses of the Older gneiss series and the younger granodiorite-adamallite series.
- (2) Dolerite dykes and sills.

#### 2.2.1 Precambrian granites and gneisses

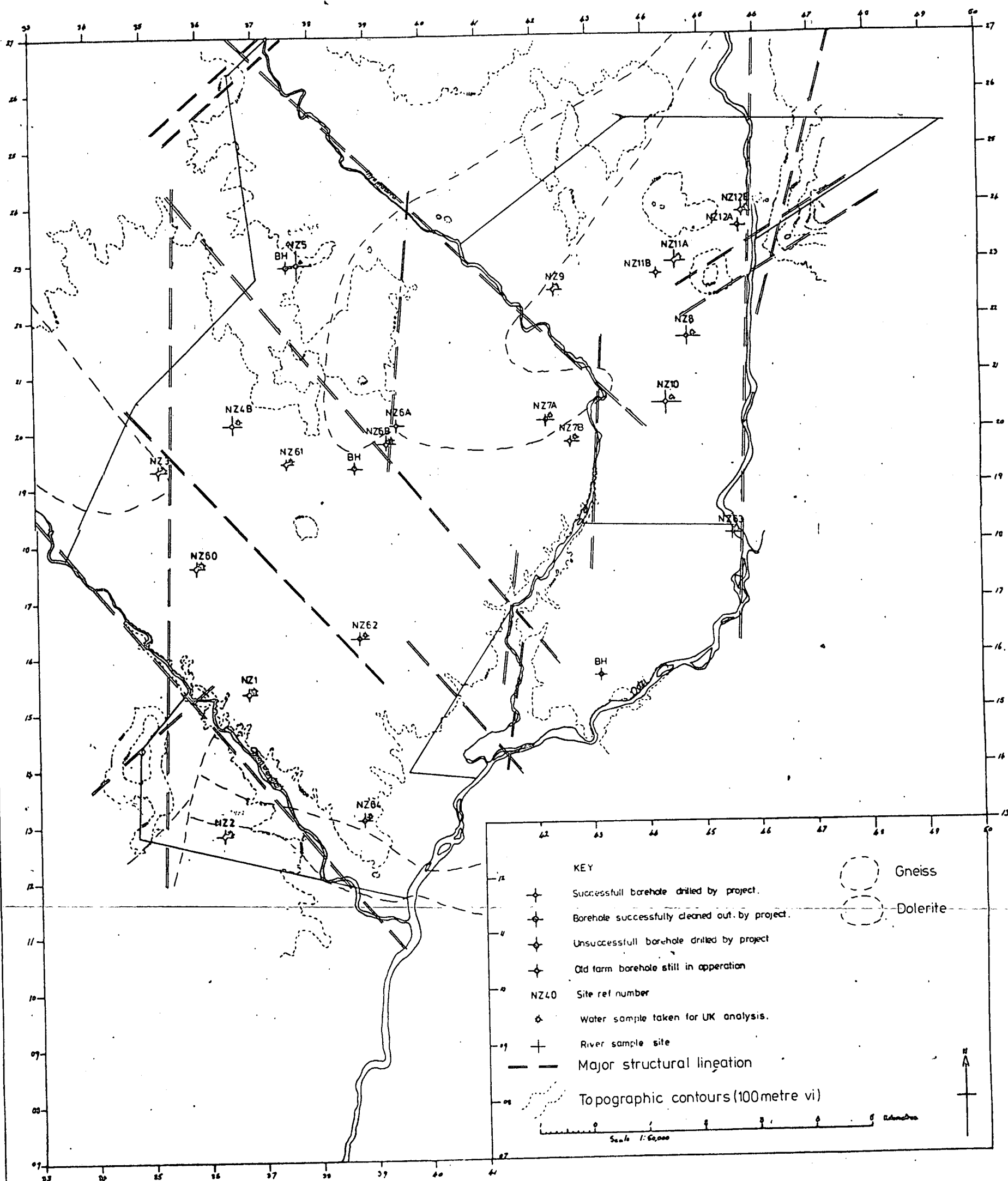
Most of the area is underlain by granites and gneisses of Precambrian age. Except in the north east of the area the strata appear to be quite uniform in type being composed of white quartz and feldspar with varying proportions of mafic minerals. These rocks are usually quite coarse grained. Sometimes rock with predominantly pink feldspars occur commonly as vein material within the white granitic gneiss.

Within the north east corner of the area more schistic strata are found alternating with white to grey coarse grained gneiss. The schistose bands are



# INYAMAZURA RESETTLEMENT SCHEME

Fig No 3 GEOLOGICAL MAP



commonly formed of dark green micaceous amphibolitic schists. Within the north east of the area these latter rocks form high hills whereas the rest of the area is underlain by the older granites and gneisses is topographically subdued.

### 2.2.2 Precambrian dolerites

Dolerites of Precambrian age occur along two east-west trending bands within the central and southern parts of the area. They commonly crop out as low ridges and occasionally high hills with a litter of rounded dark green dolerite blocks scattered at their margins. The soil cover developed upon these dolerite ridges has a characteristic bright brick red hue. These dolerites are younger than the surrounding granites and gneisses into which they have been intruded.

### 2.3 Structural Geology.

An analysis of topographic maps and aerial photography of the area has indicated the presence of a rectilinear series of fault/joint lineations that traverse the area. These lineations trend NW-SE, NE-SW and N-S, forming zones of weakness that are now followed by the main rivers of the area (see Fig. 3).

### 2.4 Borehole Siting.

Where new water supply boreholes were required to be drilled, geophysical methods were employed in association with aerial photograph interpretation, to locate the sites. Two geophysical methods were utilised:-

- (1) Electrical resistivity utilising a Wenner spread arrangement.
- (2) Electromagnetics (EM) using a 20 or 40 metre spread length.

The resistivity method is a well tried and proven method which suffers from several disadvantages:

- (a) relatively slow survey speed compared with the EM method,
- (b) lack of definition in the latter part of the curve made the calculation of depths of weathering difficult to undertake.

Therefore use was mainly made of the EM method with which rapid traversing of fairly large areas could be undertaken in relatively short periods. The contour maps produced can indicate lineations, zones of weathering, the presence of ferro-mag mineral rich rocks etc. Several examples of survey results obtained from the Nyamazura area are included in Appendix II.

Generally the higher the EM effect the greater the depth of weathering. Using this criteria three or more boreholes were located upon dolerite dykes and sills where the EM effect reflected the large amount of ferro-mag minerals present in the strata. Similarly high EM measurements (>25 millivolts) have also been obtained from amphibolitic gneisses and schists. Therefore the counterpart hydrogeologists undertaking the EM surveys were encouraged to undertake a grid survey of at least 6 lines at each site, to allow adequate contouring of the site, to note the soil colour at the site and the solid geology of and outcrops at site before selecting a drill site.

Reinterpretation of the results obtained from the surveys using the drilling results have indicated that:-

- (1) Readings of <10 millivolts generally indicate the presence of hard to solid rock near surface.
- (2) Readings of >20 millivolts indicate the presence of ferro-mag conductive minerals within the surface weathered layers derived from dolerites, amphibolitic gneisses or schists etc. and that additional data must be obtained about the solid geology before a drill site can be located.
- (3) Readings of 10-20 millivolts can generally be regarded as good indications of adequate weathering although due regard has to be made to any other geological data derived from the area. If possible Electrical Resistivity VES probes should be undertaken at the favourable site.

Of the surveys detailed in Appendix II that at village 12 (NZ2) is typical of condition 3 where a successful borehole was drilled upon an EM effect of 14.5 millivolts. That at village 7 shows the contrast between high EM effects (>25 millivolts) measured over dolerite (where an unsuccessful borehole, NZ6A, had already been drilled) and the optimum levels of <20 millivolts obtained from a lineation that turned out to be a waterlogged zone of faulted granitic gneiss. The results of the survey at village 6 again shows the contrast between a dolerite (upon which an unsuccessful borehole, NZ7A, had already been drilled) and an area further downstream where a successful hole was drilled upon an EM effect of 11 millivolts. Various NW-SE trending lineations are also located. The last example was at village 1A where a borehole was drilled into an area where the EM effect was greater than 25 millivolts. This borehole was drilled into water bearing amphibolitic gneisses and schists whose EM effect is much the same as dolerite.

### 3. HYDROGEOLOGY

#### 3.1 Introduction.

Prior to the start of the project ten boreholes had been located within the project area. No data existed from these or any unsuccessful borehole that may have been drilled in the area. No hydrogeological study had been made of the Nyamazura area or adjacent areas prior to the current study being undertaken. For the purposes of the current study hydrogeological data was obtained from thirteen holes drilled and three holes cleaned out during the study. Additional hydrochemical data were obtained from four still operational old farm boreholes.

#### 3.2 Current Studies.

During the current study the following classes of data were collected.

- (a) Geological data during borehole drilling.
- (b) Aquifer parameter data during pumping tests.
- (c) Hydrochemical data during pumping tests and spot sampling exercises.

These data were used to produce an idea of the nature of the weathered Pre-cambrian Basement aquifers within the Nyamazura area.

### 3.3 Geological Data.

A series of thirteen boreholes were drilled using Dando cable tool percussion rigs and a Hands England HE20 down-the-hole hammer rig within the Nyamazura area. Where possible these holes were drilled to a minimum diameter of 152 mm (6 inch) and completed at 110 mm being lined from top to bottom with 110 mm diameter Protorite PVC casing and screen. This screen was gravel packed with a sanitary seal of cement being poured from ground surface to a depth of 5 metres above the pack material. During drilling, sludge samples were collected and logged geologically at one metre intervals. The driller recorded the relative hardness of the strata penetrated, changes in colour, location of fractures, changes in rest water levels and depths of zones of water production. The sludge samples collected were stored in glass sample bottles for future analysis. Geological logs, driller's logs and borehole construction logs are recorded and presented in Appendix III.

### 3.4 Pumping Test Data.

Of the sixteen boreholes drilled or cleaned out during this study twelve were subjected to one form or another of pumping test. At the initial hole to be tested, NZ4B, a 6-hour constant yield/drawdown test was undertaken followed by a 1 hour recovery test. Due to time constraints the constant yield/drawdown test was reduced to 3 hours duration with a one hour recovery test. Such a test procedure was used at NZ5, NZ8, NZ9, NZ10 and NZ6B. Reduced time period tests were conducted at NZ7A, NZ11A and NZ12A where poor yields were encountered during testing. Latterly in an attempt to reduce testing time even further a standardised bail test was introduced. This involved bailing the hole using cable tool percussion equipment for a period of 30 minutes and recording the maximum drawdown level and recovery over a 60 minute period. This form of test was undertaken at NZ6B, NZ11B and NZ12B. When plotted upon semi log paper the recovery data from the bail tests and from the longer term constant yield tests appear to be in fairly good agreement especially the long term data where the bail test results for  $t/t' < 2$  are noted (see Fig. 4).

The constant yield/drawdown data were analysed using the Jacob Straight Line Method while the recovery data obtained from these and the bail tests were analysed using the Theis Recovery Method. In general there was good agreement between the results obtained from both methods once the effects of well storage had been overcome. The transmissivity values obtained from the bail tests were usually on the low side, there being insufficient "late" data available to allow adequate analysis of the results in most cases. The results are presented in Table 1, and in Appendix IV.

The results obtained indicated that the dolerite sills and dykes have very low transmissivities below their initial very weathered upper layers. T values of less than  $0.1 \text{ m}^2/\text{day}$  were recorded at three sites indicating that for throughflow analysis purposes the dolerites can be regarded as being impermeable blocks. Within the weathered basement complex aquifers T values were lowest within water shed areas, e.g. at NZ5 where T values of  $< 10 \text{ m}^2/\text{day}$  were recorded. T values increased down the hydraulic gradient to  $> 20 \text{ m}^2/\text{day}$  in the vicinity of the main rivers.

### 3.5 Hydrochemical Data.

Hydrochemical data were obtained from two primary sources:

- (a) pH, temperature and conductance of groundwater pumped were measured at regular intervals during pumping tests.

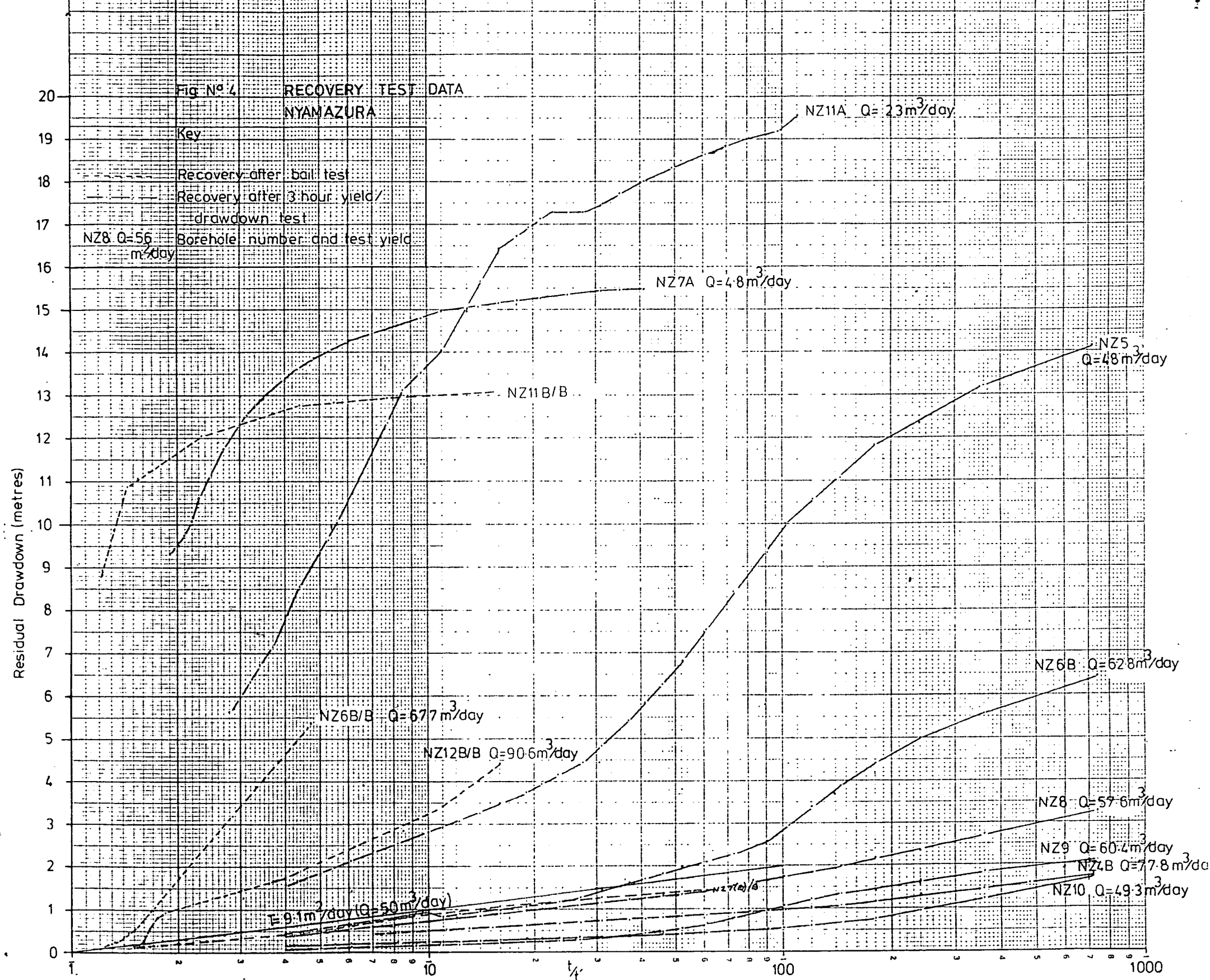


TABLE 1. PUMPING TEST RESULTS, JUNE-AUGUST 1984 - NYAMAZURA.

Borehole No.	Date	Type of Test	Test Duration (minutes)	Method of Analysis	Transmissivity (m <sup>2</sup> /day)	Specific Capacity (m <sup>3</sup> /day/m)
NZ4B	27-4-84	Yield/Drawdown	360	Jacob Straight Line	(1) 16.38	39.98
		Recovery	60	Theis Recovery	(2) 24.73 30.9	
NZ5	2-7-84	Yield/Drawdown	180	Jacob Straight Line	2.0	2.70
		Recovery	60	Theis Recovery	(1) 1.2 (2) 3.6	
NZ7A	20-7-84	Yield/Drawdown	24	Jacob Straight Line	1.16	
		Recovery	60	Theis Recovery	0.048	
NZ8	10-7-84	Yield/Drawdown	180	Jacob Straight Line	8.43	14.08
		Recovery	60	Theis Recovery	(1) 5.64 (2) 12.40	
NZ9	18-7-84	Yield/Drawdown	180	Jacob Straight Line	(1) 16.50	24.35
		Recovery	60	Theis Recovery	(1) 31.59 (2) 44.23	
NZ10	11-7-84	Yield/Drawdown	180	Jacob Straight Line	(1) 13.9	19.74
		Recovery	60	Theis Recovery	(2) 21.2 (1) 5.82 (2) 40.07	
NZ11A	16-7-84	Yield/Drawdown	115	Jacob Straight Line	(1) 1.2	0.77
		Recovery	60	Theis Recovery	(2) 0.27 (1) 1.3 (2) 0.28	
NZ12A	17-7-84	Yield/Drawdown	35		Very small	
NZ6B	2-8-84	Yield/Drawdown	180	Jacob Straight Line	(1) 5.11	8.99
				" " "	(2) 8.85	
		Recovery	60	Theis Recovery	(1) 2.05	
				" " "	(2) 5.23	
		Bail Test	30/60	" "	(3) 8.22	
		Recovery			1.25	
NZ7B	10-8-84	Bail Test Recovery	30/60	" "	10.26	33.92
NZ11B	31-7-84	Bail Test Recovery	30/60	" "	0.017	<6.28
NZ12B	9-8-84	Bail Test Recovery	30/60	" "	5.72	20.26

- (b) A total of eighteen samples were taken from boreholes and the Odzi river for analysis in the UK. Groundwater pH, temperature, conductivity and bicarbonate content were determined at each sample site. Each sample was taken in two parts, one remained non-acidified while the other was acidified using concentrated hydrochloric acid. The results of these analyses are still awaited at the time of writing.

#### 4. RESULTS

##### 4.1 Nature of the Weathered Basement Aquifer System.

From the geological logs obtained from boreholes drilled in the area the typical sequence through the weathered zone from ground surface to solid rock would be a profile such as that illustrated in Fig. 5. Within this profile the upper weathered zone would develop within the zone of maximum water movement, i.e. rainfall recharging the aquifer passes through the zone and the water table oscillates within that zone during normal to wet climatic periods. Therefore minerals within this zone are subjected to wet-dry conditions and attack by recharge water when it is in its most acid condition. The resulting weathering is indicated by a breakdown of feldspars to clays with their removal from the near surface zone with runoff water and the oxidation of iron rich minerals with their redeposition in the near surface zone as ferricrete nodules or laterite bands.

Within the lower weathered zone the breakdown of minerals due to attack by low pH waters and wetting and drying cycles probably only takes place during near drought conditions when the water table is reduced in elevation. Within this zone ferromag minerals are initially oxidised and then removed upwards in solution by capillary action to the upper zones. The feldspar minerals are sufficiently attacked by acid water to cause them to crack but not to form clays.

The lowest zone is the relatively unweathered zone where water is contained within joints within the strata. The pH of these waters appears to have increased during their passage down through the upper weathered zones to render them non corrosive.

Within the Nyamazura area the weathered zone appears to be thickest on subdued ridges, e.g. at NZ5 where the zone of water table oscillation is greatest. There the weathered zone is in excess of 30 metres thick. However at this site the transmissivity of the saturated zone of weathering is low due to the presence of much clay in the sequence.

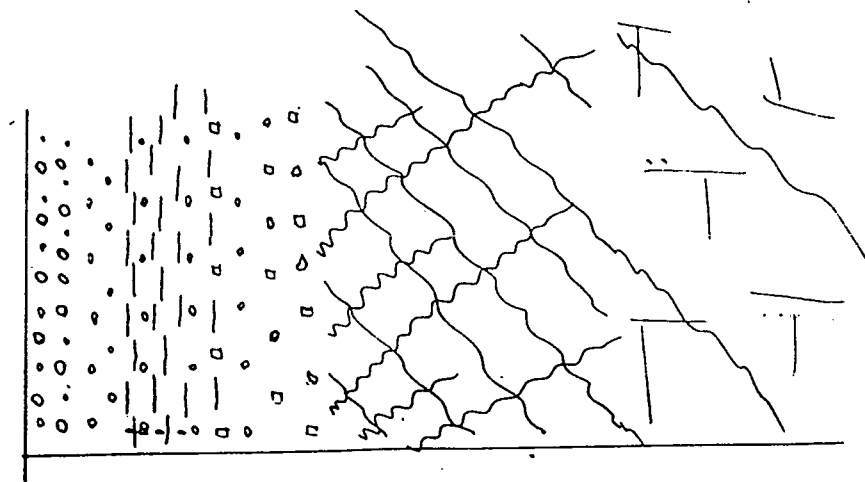
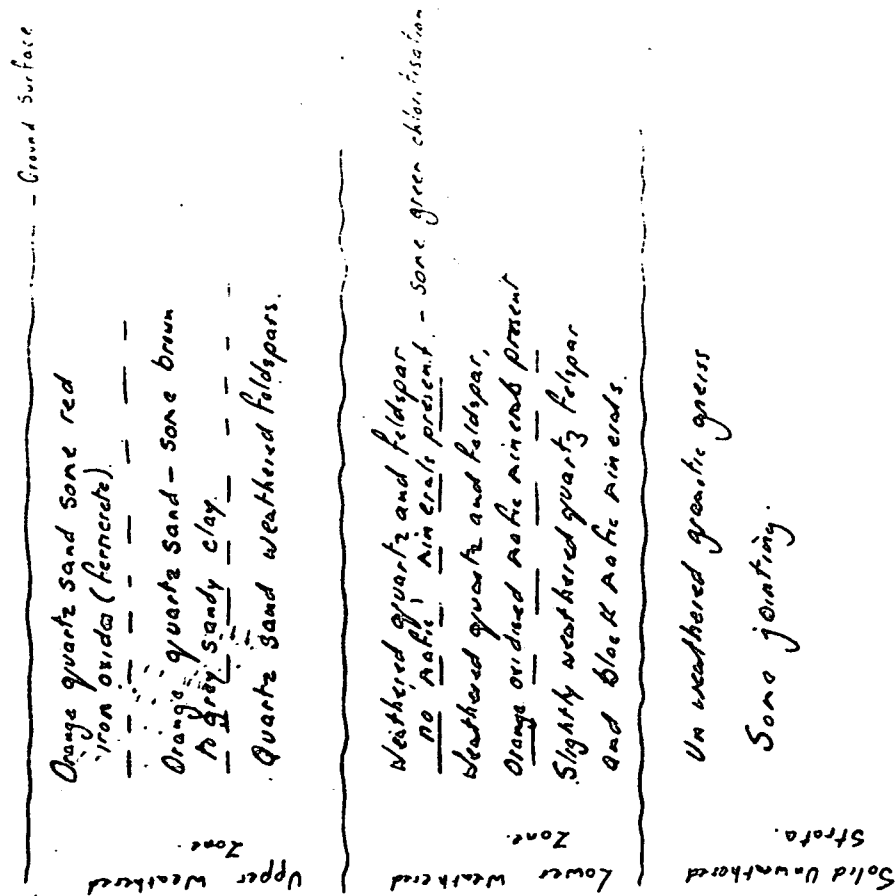
The thinnest zones of weathering are developed adjacent to the main rivers where the zone of water table oscillation is thinnest. In the area between the ridges and the rivers the zone of weathering is commonly 20 metres or more thick (see cross sections NZ5-NZ10 and NZ2-NZ5 (Fig. 6 and 7)).

Due to the small number of pumping tests undertaken within the Nyamazura area a comprehensive distribution map of transmissivity cannot be constructed. However there is some evidence to show that over much of the area the weathered Pre-cambrian Basement aquifer has a transmissivity of between 10 and 20 m<sup>2</sup>/day.

What is evident is that the zone of weathering is enhanced along fault and prominent joint lineation zones, e.g. at NZ6B. Within the dolerites the upper weathered zone is evident to a great degree as seen in several boreholes where

Fig N° 5

Typical Weathered Rock Profile for Coarse Grained Feldspathic Granitic Gneisses



Solid well jointed gneiss



Fig N96 HYDROGEOLOGICAL CROSS SECTION NZ5E-NZ10  
NYAMAZURA

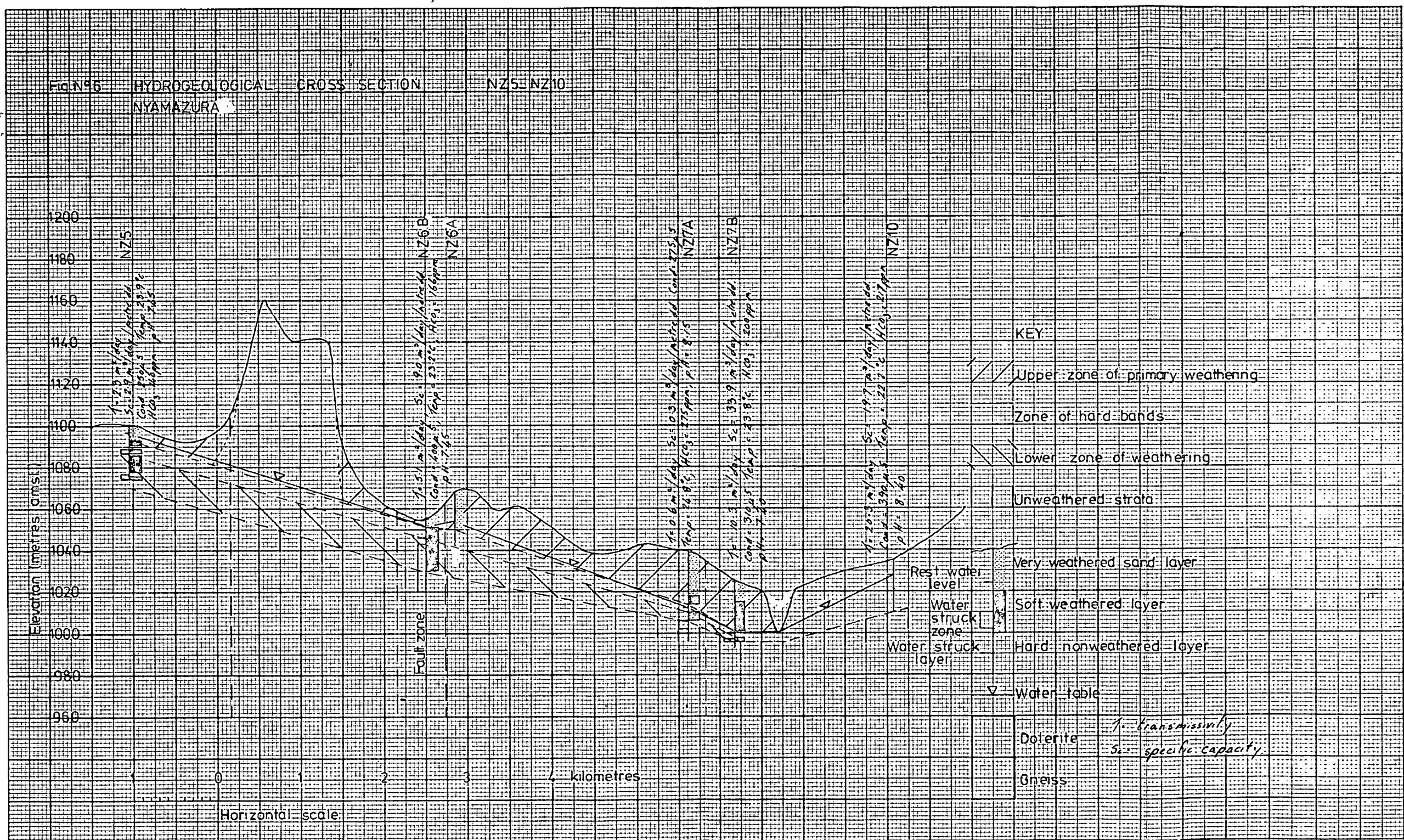
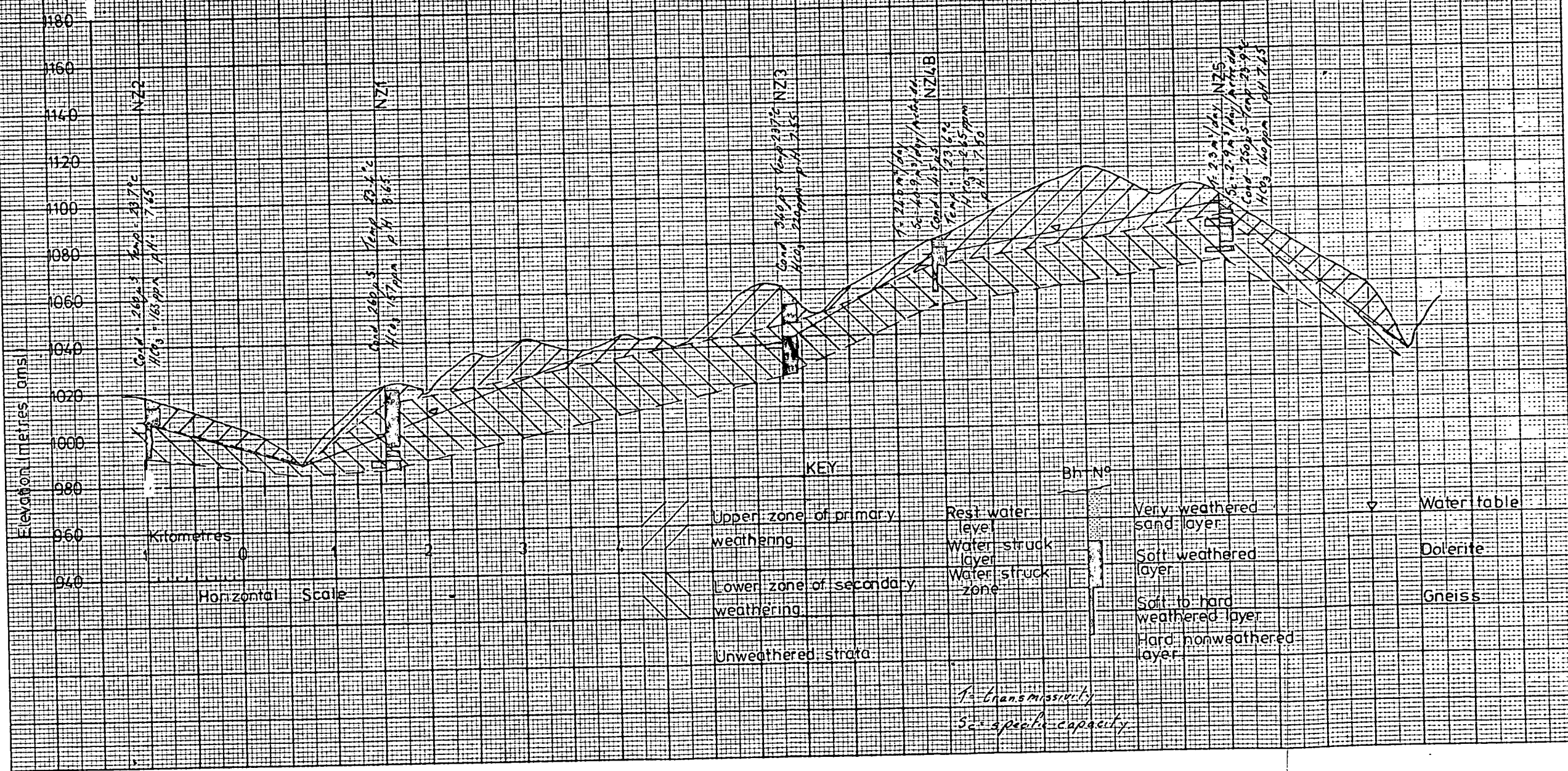


Fig No 7 HYDROGEOLOGICAL CROSS SECTION NZ2 — NZ5  
NYAMAZURA





the dolerite has decomposed to a green-brown sand. Below this upper layer however the dolerite remains quite solid with zero permeability except for very thin weathered zones which appear to coincide with the lower zone in the granitic gneisses. These thin weathered zones contain very small quantities of water and have very low permeabilities (e.g. NZ11B).

#### 4.2 Groundwater Flow and Recharge.

Within the Nyamazura area groundwater flow is controlled by topography, structural lineations and impermeable dolerite masses, taking place mainly through the weathered Basement Complex aquifer zone (see Fig. 8). Groundwater appears to move from the ridge areas of recharge down dip towards the rivers into which it flows. This general pattern of flow is altered by major structural lineations and by runoff from dolerite hills as is indicated by the groundwater conductance distribution map (see Fig. 8). Rain water runs off the dolerite hills southeast of Game Valley to enter the weathered basement aquifer and flow due south to the Chingwandow valley to the south. Meanwhile the groundwater within the aquifer to the south east of the hills is much more static in nature as indicated by the higher groundwater conductivities recorded ( $>400 \mu\text{S}$ ).

The hydrochemical results so far obtained would tend to support this view of groundwater flow in the Nyamazura area. pH values of  $<7.5$  are found around the southern margin of the dolerite block to the south east of Game Valley indicating that runoff of rainfall water probably occurs from the dolerite block onto the granitic gneiss. pH is seen to increase down dip towards the Chingwandow valley in the direction of flow (see Fig. 9).

In the same area bicarbonate concentrations are lowest along the western margin of the same dolerite block supporting the view that groundwater flows from that area to the south.

In the north east of the area transmissivity values are much less along the flanks of a steeply-sided ridge. Both pH and bicarbonate values increase rapidly down dip towards the Inyamazura river. Very low values are recorded to the east along the banks of the Odzi river probably due to mixing of groundwater and river water.

#### 5. SUMMARY

The occurrence of groundwater within the Nyamazura area has been summarised in Fig. 10. The structural fault/joint lineations, major rivers and prominent dolerite masses are seen to have marked controlling influences upon the nature of groundwater flow in the area. Factors that control the degree of weathering of the Pre-cambrian Basement Complex aquifer include the climatic regime of the area and the susceptibility of the granitic gneiss formation to weathering especially the feldspar component.

# INYAMAZURA RESETTLEMENT SCHEME

Fig. No 8 HYDROGEOLOGICAL MAP

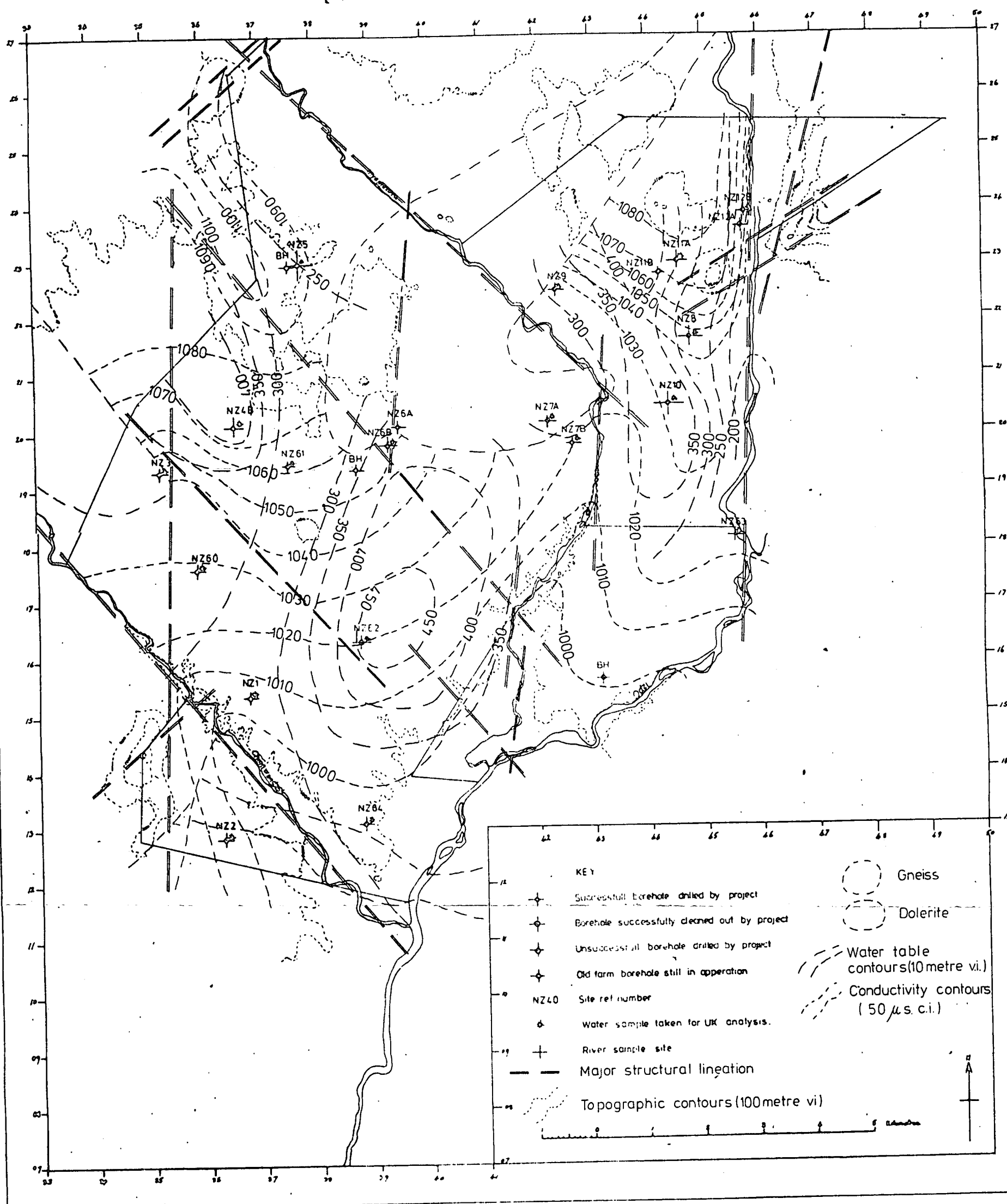
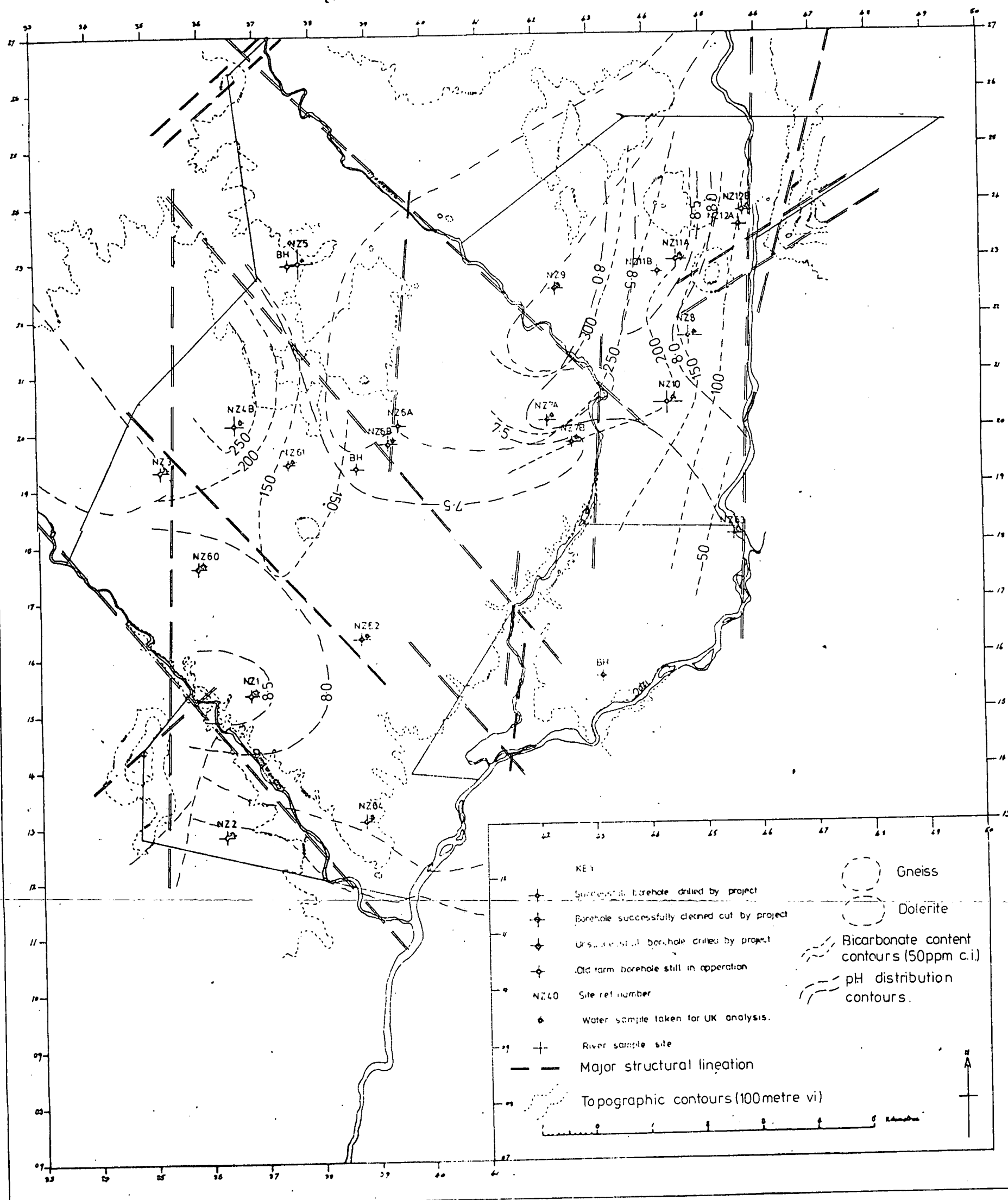
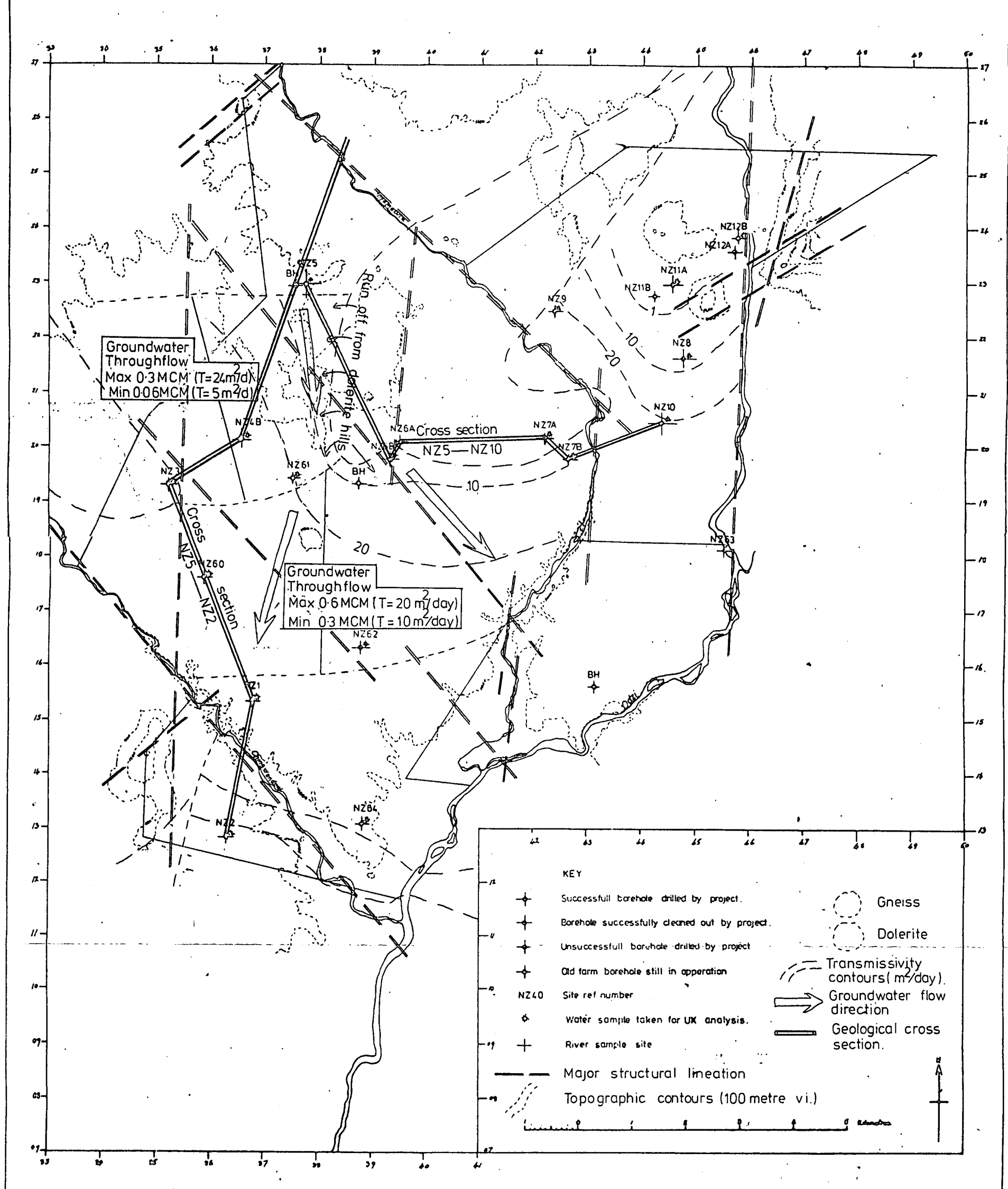


Fig. No 9 pH AND BICARBONATE DISTRIBUTION CONTOUR MAP.



# INYAMAZURA RESETTLEMENT SCHEME

Fig N°10 POSSIBLE OCCURRENCE OF GROUNDWATER WITHIN THE WEATHERED BASEMENT STRATA



A general transmissivity of 10 to 20 m<sup>2</sup>/day has been postulated for most of the Basement Complex aquifer system. Transmissivity is seen to increase radially to the south away from the southern margin of the main dolerite masses. Groundwater gradients are fairly high. Throughflows of groundwater in the Nyamazura area have been calculated. In the north west of the area groundwater throughflow is of the order of maximum 0.3 MCM/annum to minimum of 0.06 MCM/annum. Within the central part of the area groundwater throughflow is estimated to be maximum 0.6 MCM/annum and minimum 0.3 MCM/annum (dependent upon the T value selected).

The hydrochemical data so far analysed indicate that the groundwaters of the Nyamazura are of good enough quality to be used for domestic and agricultural purposes. This situation could change when the detailed chemical analyses of the water samples obtained become available. The distribution of fluoride within the aquifer system is of particular interest.

#### Acknowledgements.

The author of this report J Davies (Hydrogeologist) would like to acknowledge:

- (i) the kind help and assistance that he received from all his colleagues at the Ministry of Water Resources and Development particularly Mr D A Whitaker (PWSU Team Leader), Mr M Sharp (Drilling Supervisor) and Miss I A Richardson (PWSU Field Hydrogeologist),
- (ii) the advice of and helpful discussions with Dr E P Wright (BGS) and Dr R Herbert (BGS),
- (iii) the analytical expertise and advice of Miss J Cook (BGS),
- (iv) the typing expertise and patience of Mrs C Cordery (BGS).

APPENDIX I  
DATA SOURCES

1. Topographic maps.

Scale 1 : 50 000      ODZI 1832 C4,      UMTALI 1832 D3

Scale 1 : 250 000      Mutare sheet SE-36-10.

2. Aerial Photography.

Umtali South 1975

579-586

660-670

744-752

824-828

3. Reports.

(a) Agritex, March 1983. INYAMAZURA Intensive Resettlement. Planning Branch,  
Dept. of Agriculture and Extension Services.

(b) Swift, W H (1972). The Geology of the Odzi Golden Belt. Bull. No. B45  
Southern Rhodesia Geological Survey.

4. Geological Maps.

1 : 1 000 000 scale      National Geological Map of Zimbabwe, 1977.



## APPENDIX II

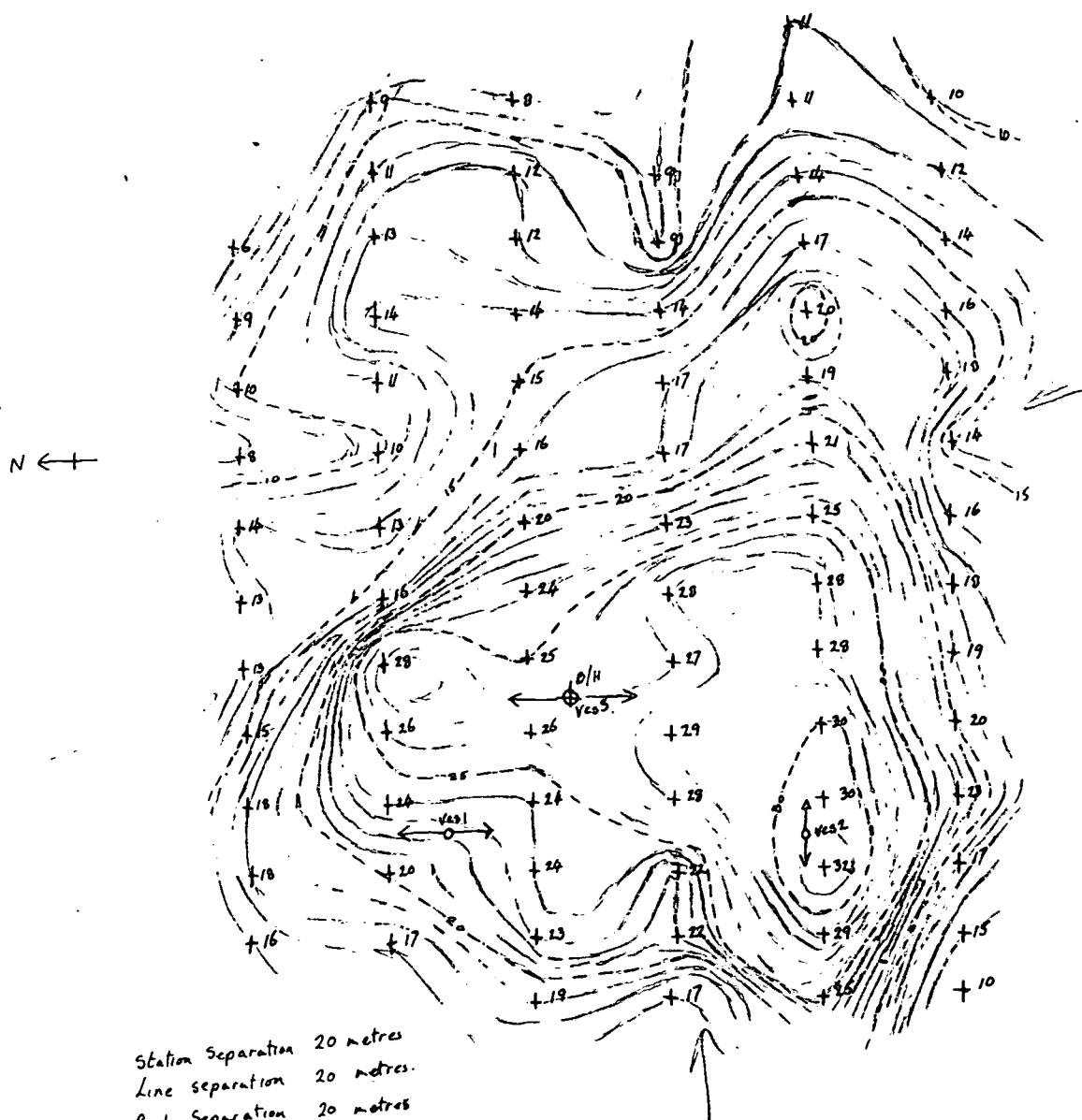
### EM RESULTS

- |    |                |                   |
|----|----------------|-------------------|
| 1. | Village No. 1A | Borehole No. NZ9  |
| 2. | Village No. 6  | Borehole No. NZ7B |
| 3. | Village No. 7  | Borehole No. NZ6B |
| 4. | Village No. 12 | Borehole No. NZ2  |

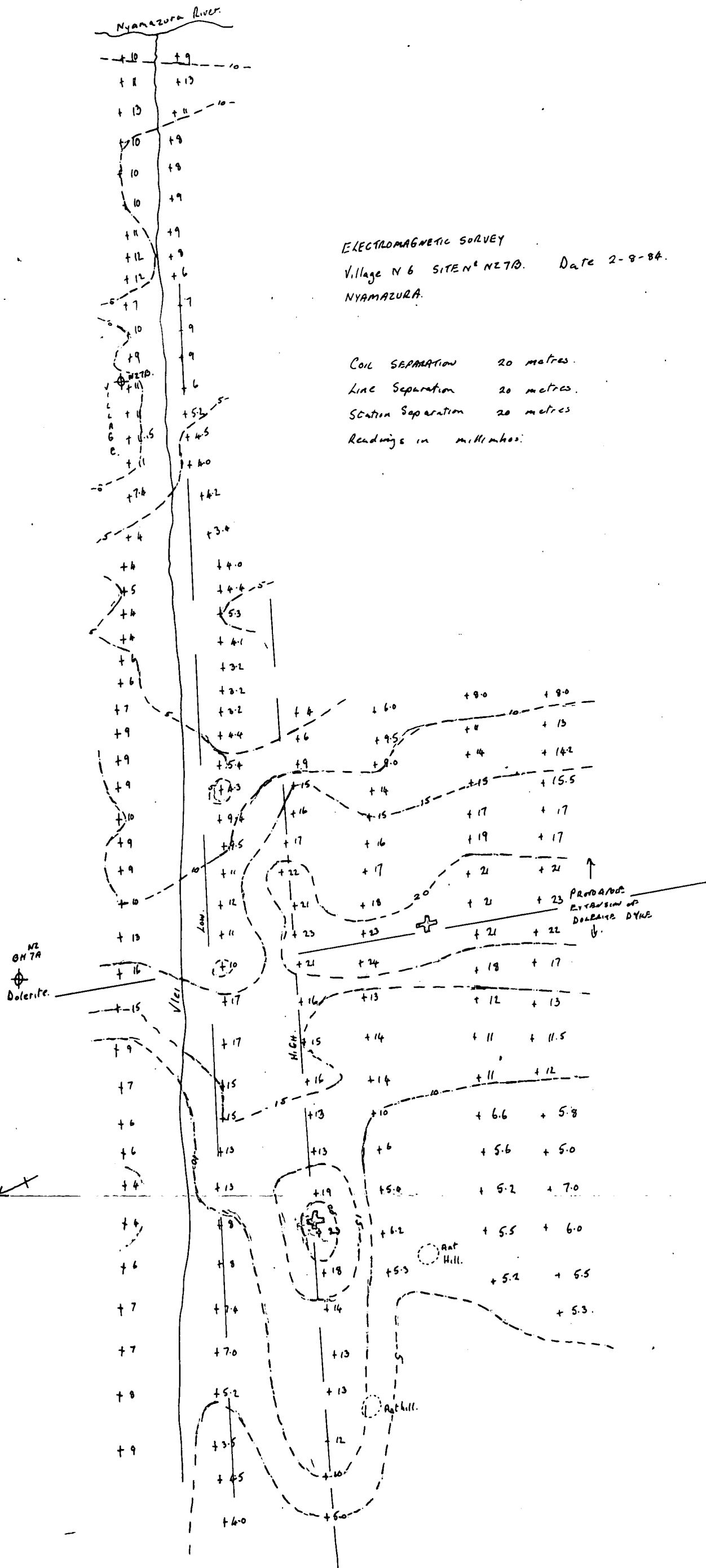
# ELECTROMAGNETIC SURVEY.

Village 1A Berchale N° NZ9 Nyanazura

Date 3/7/84.



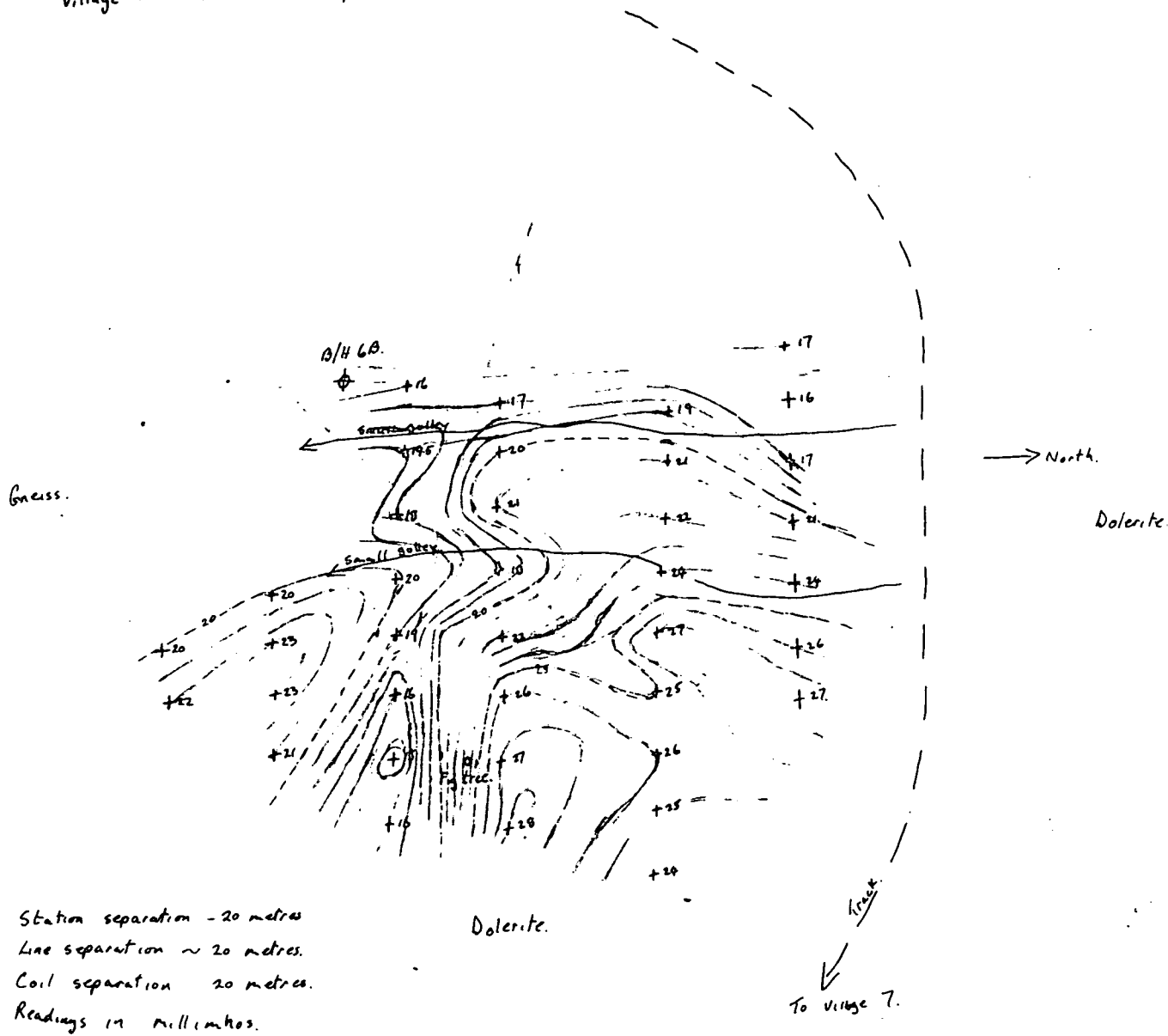
Station Separation 20 metres  
Line separation 20 metres.  
Coil Separation 20 metres  
Readings in millimhos.



# ELECTROMAGNETIC SURVEY

Village 7 Site NZ 6A Nyamazura.

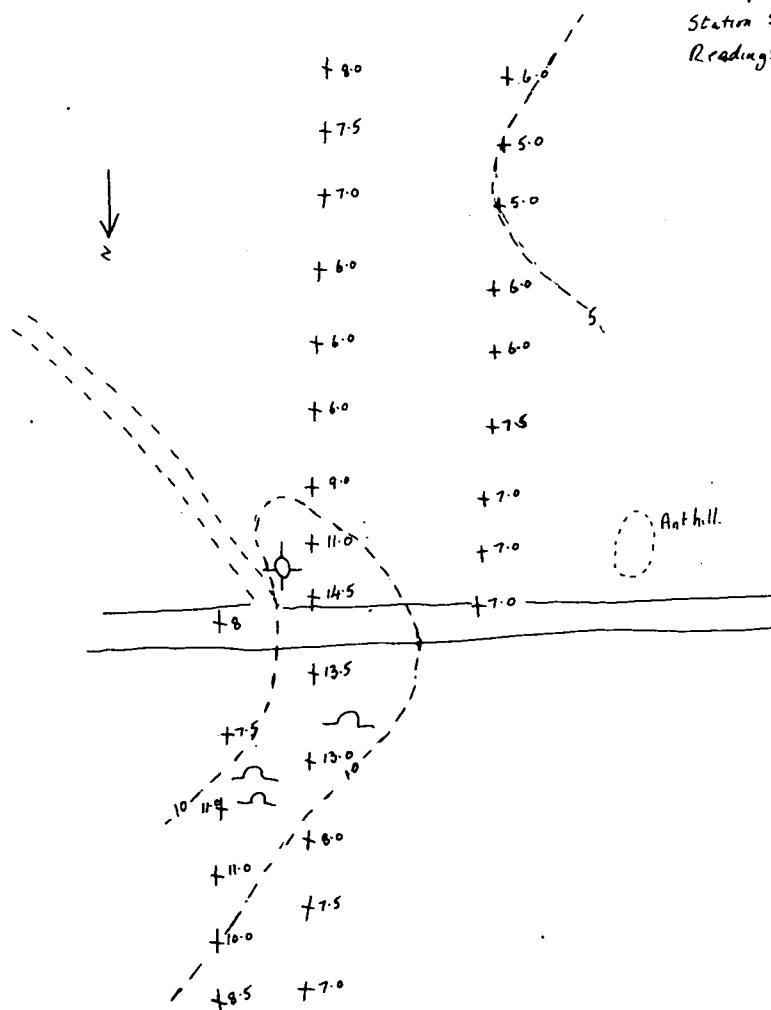
Date 4/7/84.



# ELECTROMAGNETIC SURVEY

Village 12 NZL. NYAMAZURA 22-5-84

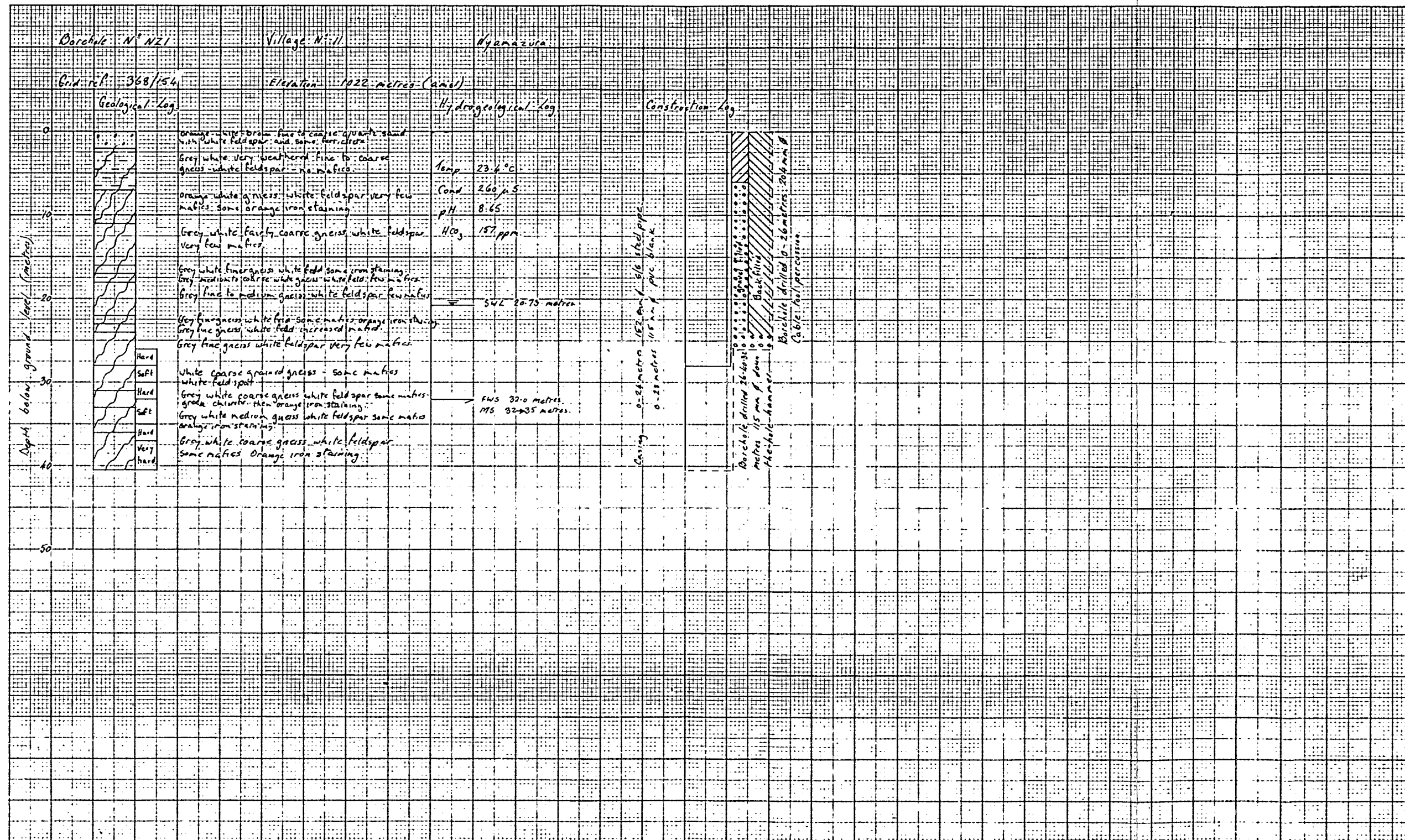
Coil separation 40 metres  
Station separation 20 metres.  
Readings in millimhos.



# APPENDIX III

## BOREHOLE LOGS

1	-	NZ1
2	-	NZ2
3	-	NZ3
4	-	NZ4A
5	-	NZ4B
6	-	NZ5
7	-	NZ6A
8	-	NZ6B
9	-	NZ7A
10	-	NZ7B
11	-	NZ8
12	-	NZ9
13	-	NZ10
14	-	NZ11A
15	-	NZ11B
16	-	NZ12A
17	-	NZ12B



Borehole N° NZ.2

Village N° 12

Nyamazura

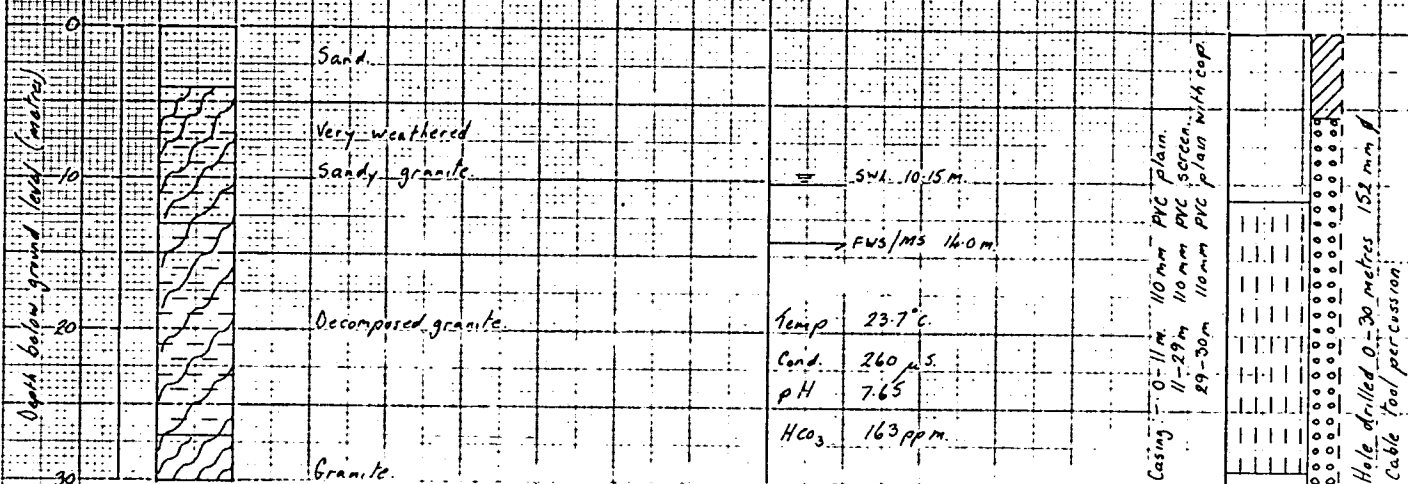
Grid Ref. 363/128

Elevation 1018 metres (a.m.s.l.)

Geological Log

Hydrogeological Log

Construction Log



Notes

1. Rest water level during drilling

Date	RWL (metres)
5-6-84	10-10
6-6-84	10-15
7-6-84	10-15
8-6-84	10-15

2. Bailer Tests (5" Bailer)

Date	RWL (m)	N° of Bails	Time Taken	Drawdown to
6-6-84	10-15	30	19 mins 5 secs	18-30 m
7-6-84	10-15	21	12 mins 9 secs	14-60 m

3. Hole developed for 15½ hours by pumping



Borchgrevink N° NZ 4-A		Village N° 9		Nyamazura	
Grid ref. 345/202		Elevation 1075 metres (a.m.s.l.)			
Geological Log		Hydrogeological Log		Construction Log	
0		Hole dry			
10				Hole abandoned as dry and base filled	
20				Hole drilled 0.16 metres of 152 mm cable tool percussion	
Depth below ground level (metres)					
Hole stopped in hard granite					
Notes					
1. This hole was drilled at a site some 400 metres south of B/H N° NZ 4-B					

Bordado N° 12-40

Village N° 9

Nyamazura

Grid ref 365/201

Elevation 1080 metres (amsl)

Geological Log

Hydrogeological Log

Construction Log

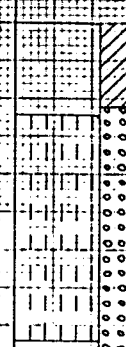
Depth below ground level (metres)



Light brown clayey sand  
White fine to medium sand  
Fine to coarse light brown sand  
Light brown weathered granitic gneiss  
Grey-brown weathered granitic gneiss  
Grey-green weathered granitic gneiss  
Weathered granitic gneiss - angular fragments of pink feldspar and white quartz, light grey in colour

SWL 5.75 m  
FWS/M 10.50 m  
Cond. 405  $\mu$ S  
Temp. 23.5°C  
HCO<sub>3</sub> 265 ppm  
pH 7.95

Casing: 0-6 m 100 mm Ø PVC screen  
6-21 m 100 mm Ø PVC screen  
21-22 m 100 mm Ø PVC screen



Hole drilled 0-22 m 152 mm Ø  
Cable tool percussion  
30 bags of gravel

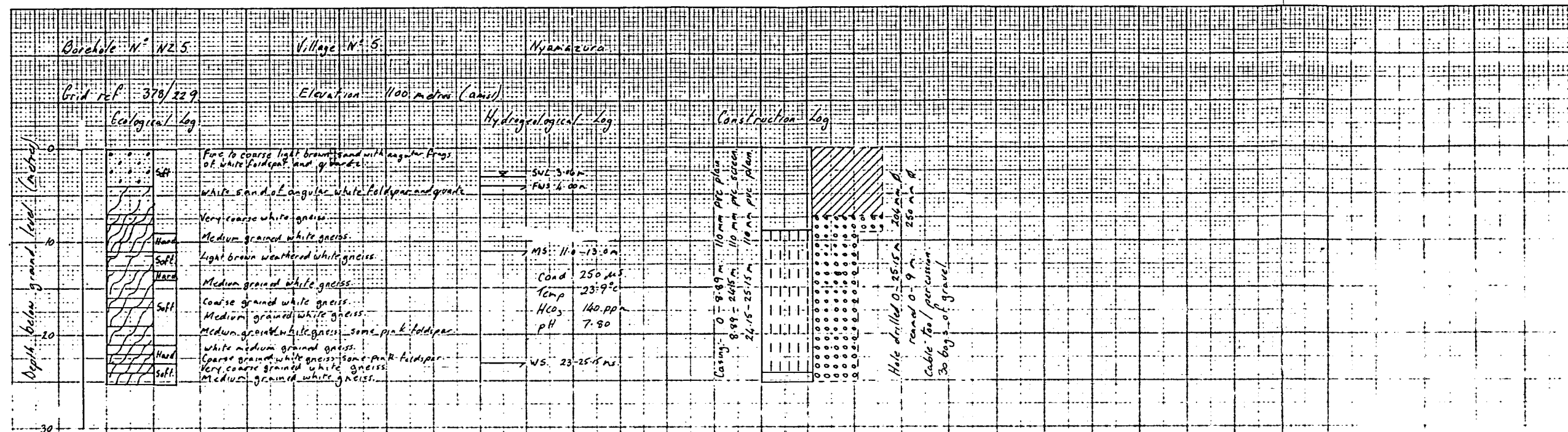
Notes

1. Rest water levels during drilling

2. Barker tests (372 barker)

Depth (metres)	RWL (metres)
13	7.95 m
18	6.31 m
21	5.86 m
22	5.92 m

Depth	RWL	N° of Barts	Time taken	Drawdown to
13	7.95	30	16 mins	10.85
18	6.31	20	10 mins	?



#### Notes

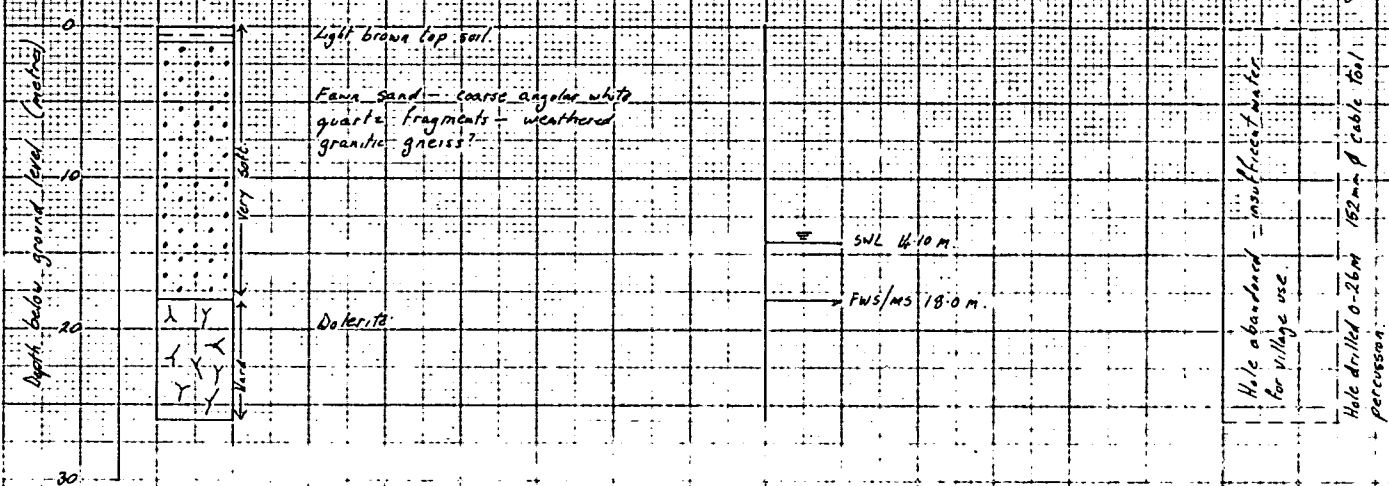
##### 1. Rest water levels during drilling

Date	Depth (m)	RWL (m)
18-6-84	8.65	3.06
19-6-84	16.00	3.18
20-6-84	21.00	3.06
22-6-84	25.15	3.10

Нысанзұра

Elevation - 1068 metres (and 1)

## Construction Log



1. Rest water levels during drilling

Rev. (continued)

14-40

14-10.  $\alpha$



Borehole N° NZ 60

Village N° 7

Nyamazera

Grid ref. 3.93/1.98

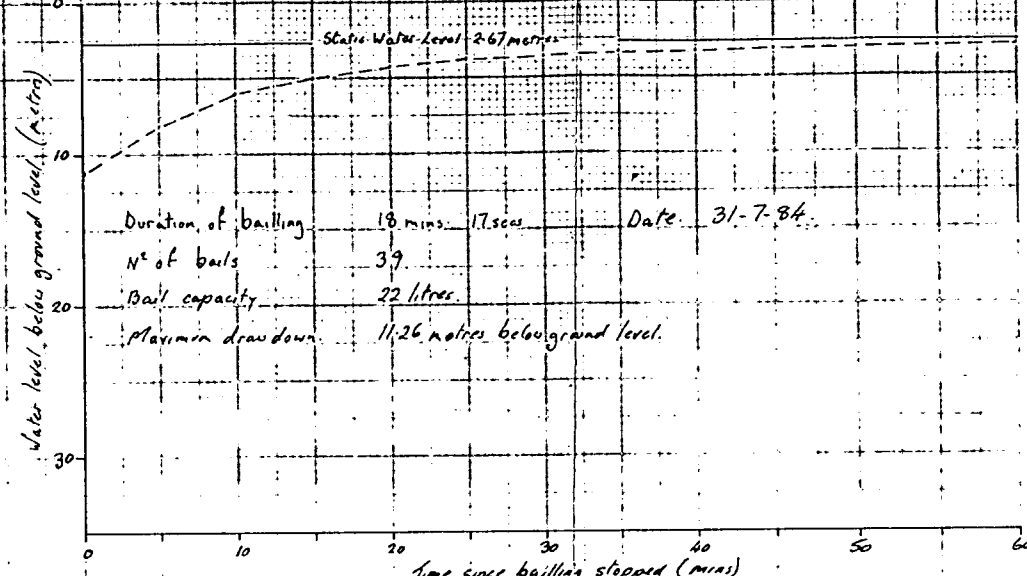
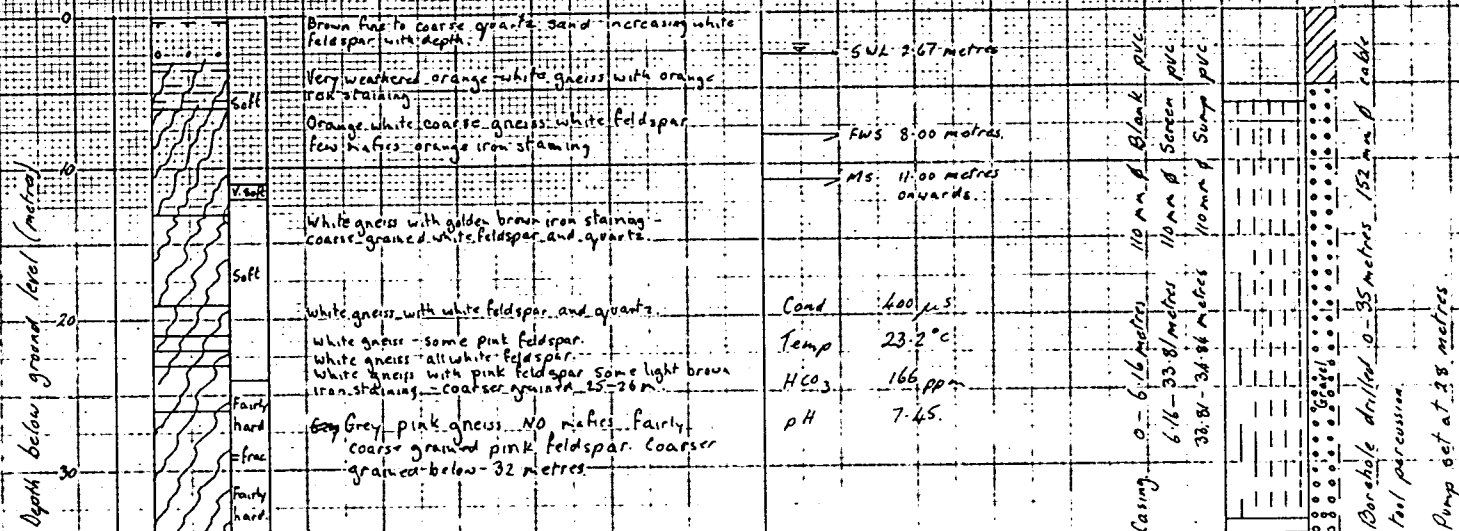
Elevation 1055 metres (approx)

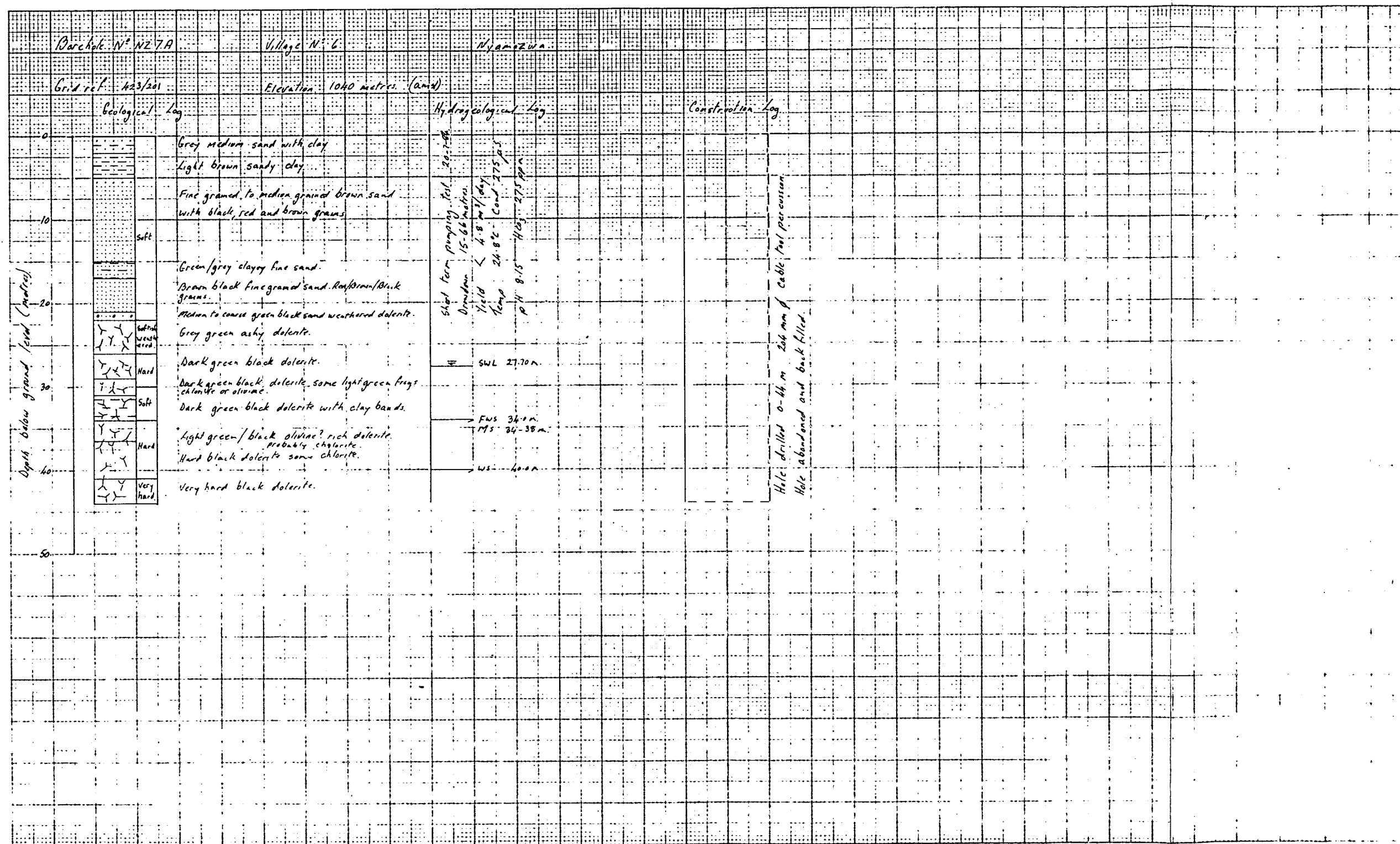
Geological Log

Hydrogeological Log

Construction Log

Recovery data





Bore hole N° NZ 73

Village N° 6

Nyamagusa

Grid ref. 426/197

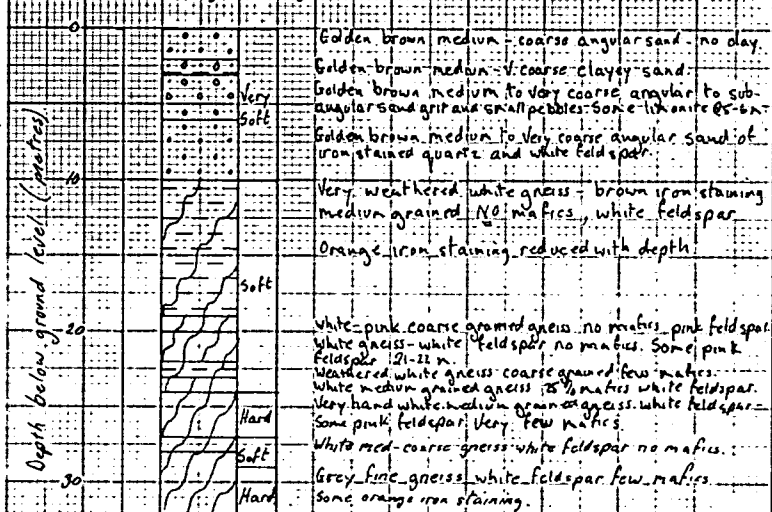
Elevation 1045 metres (and)

Geological Log

Hydrogeological Log

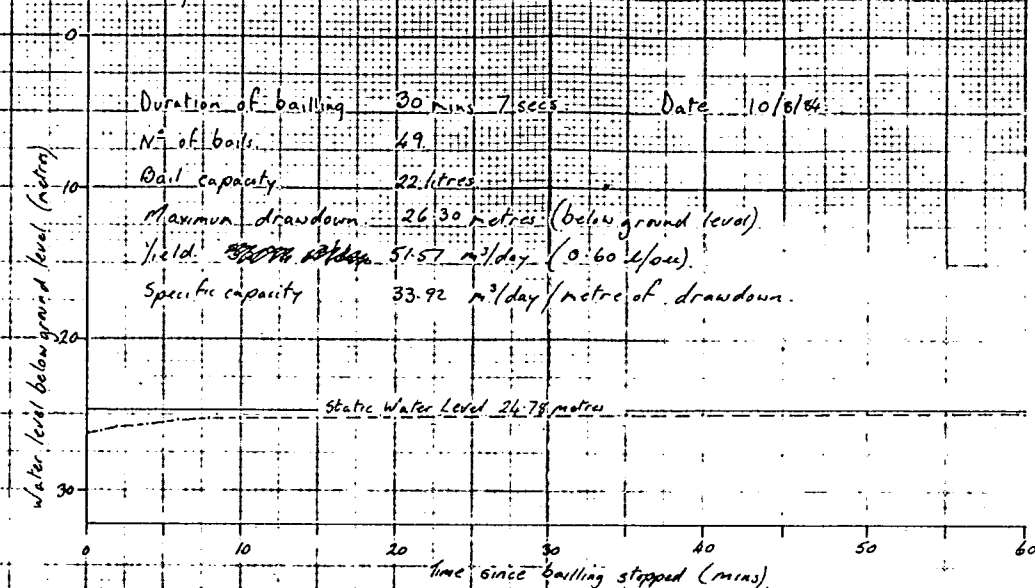
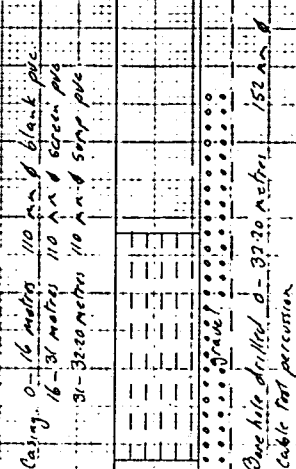
Construction Log

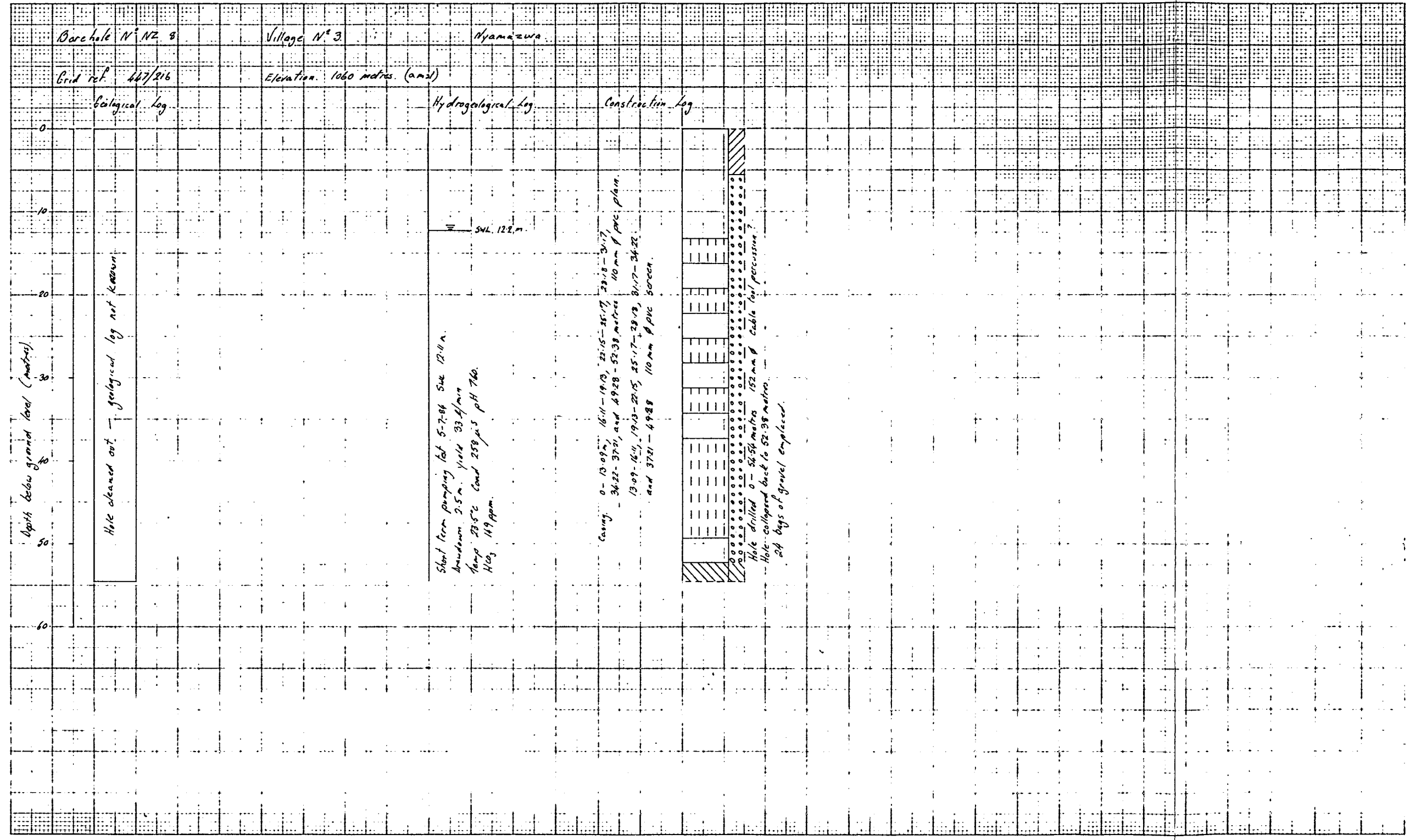
Recovery Data



Temp 26.2°C  
Cond 320 µs  
pH 7.35  
HCO<sub>3</sub> 200 ppm

SWL 24.78 metres.

FWS 28.0 metres.  
WS 29.0 metres.





Borehole N° 129

Village N° 1A

Nyamazura

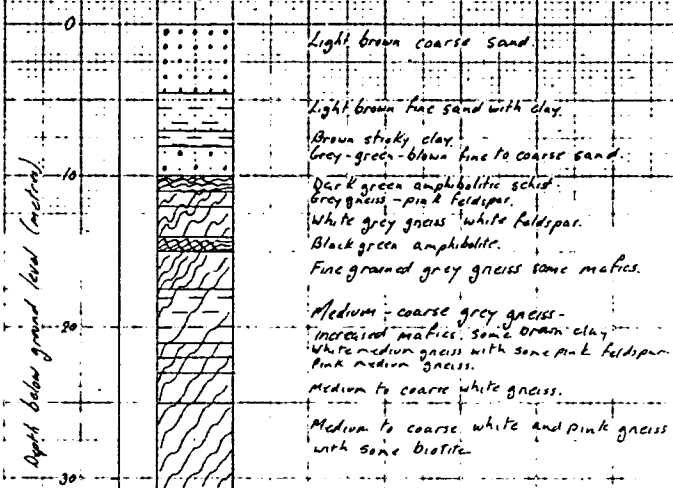
Grid ref. 424/225

Elevation 1065 metres (a.s.l.)

Geological Log

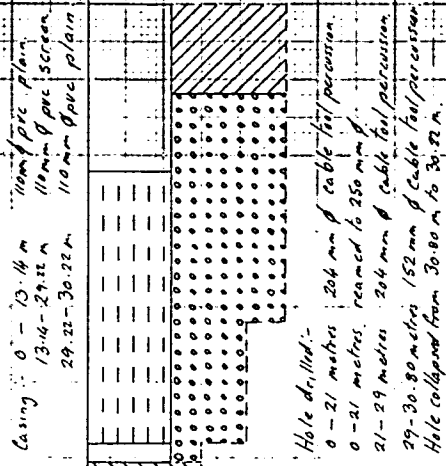
Hydrogeological Log

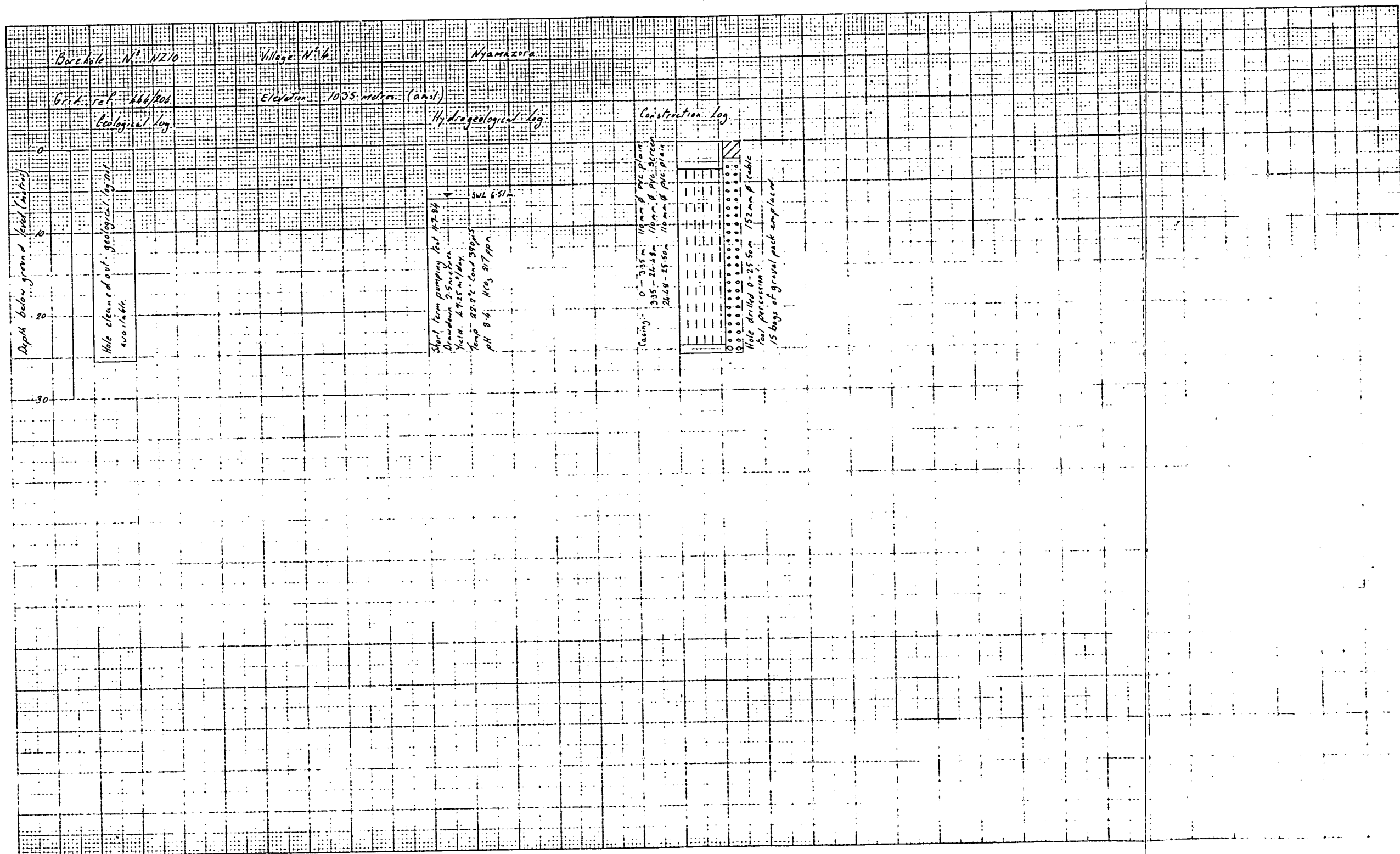
Construction Log



SWL 19.6m.  
FWL 21.0m.

Short term pumping test, 18/7/84.  
Drawdown 2.48 metres.  
Yield 60.4 m<sup>3</sup>/day.  
Temp 24.0°C Cond 320 µS.  
pH 7.80 HCO<sub>3</sub> 320 ppm.





Barchali N. N. 2. 4. A.

Village N. 2.

Nyamazura

Grid ref. 665/229

Elevation 1077 metres (and)

Geological Log

Hydrogeological Log

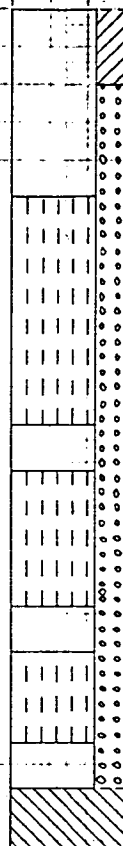
Construction Log

Depth below ground level (metres)

Hole closed out - Geological Log not available

Short term pumping test 16-7-84  
Drawdown ~ 20.28 metres. Yield ~ 23 m<sup>3</sup>/day.  
Temp 22.6°C Cond 325 µS. pH 8.7  
HCO<sub>3</sub> 225 ppm.

Casing: 0-12.36 m 27.44-30.46 m, 39.50-42.47 m and 48.51-51.57 m  
110 mm Ø pvc plain flush joint.  
12.36-37.44 m, 30.46-39.50 m and 42.47-48.51 m  
110 mm Ø pvc screen flush joint.



Hole drilled 0-55.48 metres. 153 mm Ø table top pressure?  
Hole collapsed back to 51.57 m, after cleaning.  
Hole abandoned 17/7/84 but left open for possible future use.

Borehole N° NZ 11/B

Village N° 2

Nyamazura

Grid ref. 462/228

Elevation 1075 metres (aasl)

Geological Log

Hydrogeological Log

Construction Log

Recovery Data After 30 min Bail Test

Depth below ground level (metres)

Soft  
Hard  
Very Hard  
Hard

Light brown sand clayey in parts  
light brown clayey sand some black brown sand  
Dark brown/black medium sand with little clay  
Black green weathered dolomite some calcite  
10-11.2; Very weathered 12-13  
Hard brown black dolomite

Swl 6.10 metres

Fws/mis 11.00 metres

Temp 26.2°C

Cond. 420 µS

pH 8.75

Borehole drilled 0-30 metres  
30 m of cable tool percussion

Water level below ground level (metres)

Date 9/1/86  
Drawdown to 19.60 metres N° of bails 21 x 37 litres Time taken 13½ mins - bailed hole dry

Static water level 6.10 metres

Time since bailing stopped (mins)

Нүамазуга

Construction Log

Hydrogeological Log

Construction Log

Cond 245  $\mu$ S.  
Temp 23.4°C  
pH 8.25

Hole drilled	Hole drilled
46-52 m.	0-6 metres
45 m	75% rock
Down the hole hammer	10/11 m

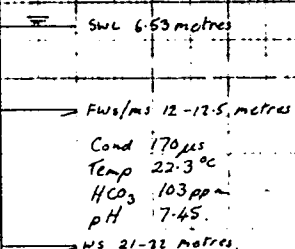
Nyamazura

Elevation.	1067 metres (anal).
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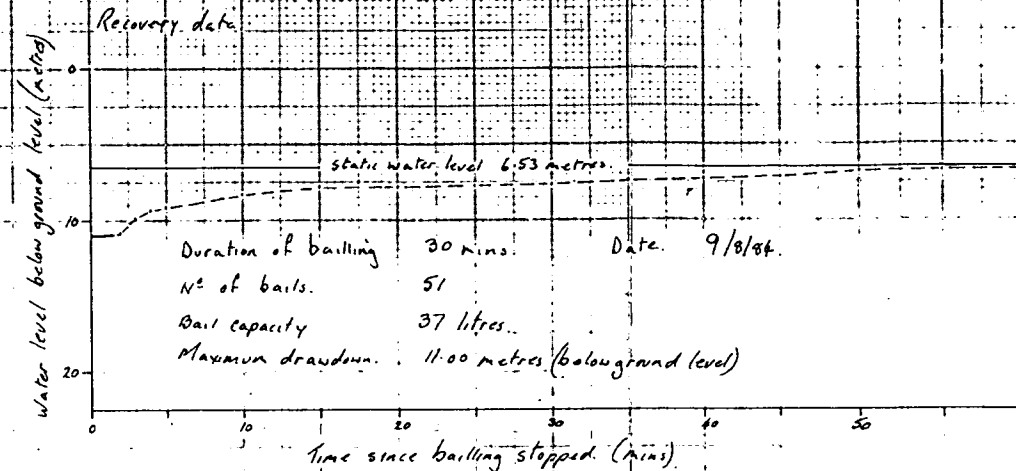
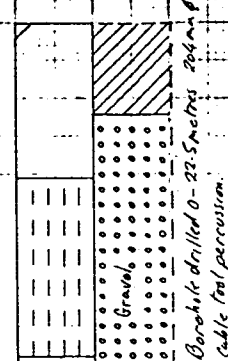
## Hydrogeological Log

16 pvc Construction Log

Recovery data



Casing 0- 10.16 metres 11mm Blank pipe  
10.14 - 22.00 metres 11mm Screen pipe  
22.00 - 22.50 metres 11mm Blank pipe



APPENDIX IV  
PUMPING TEST DATA

<u>Borehole No.</u>	<u>Village No.</u>
NZ4B	9
NZ5	5
NZ6B	7
NZ7A	6
NZ7B	6
NZ8	3
NZ9	1A
NZ10	4
NZ11A	2
NZ11B	2
NZ12A	1B
NZ12B	1B

# Constant Yield Pumping Test

Borehole N° NZ 4 (13)

Date 27-4-84

Time test started 11-00 am

Pump cylinder @ 19.64 m

Reciprocating Pump

Time (mins)	Water level (metres)	Draw down (metres)	Yield per 5 gals	Temp °C	Cond $\mu$ S	pH			
55	5.913								
57	5.915								
11-00	Pump test started								
00-15	6-11	0-195							
00-30	6-19	0-275							
00-45	6-25	0-345							
1-00	6-33	0-415							
1-15	6-40	0-495							
1-30	6-45	0-535							
2-00	6-56	0-655							
2-30	6-62	0-715							
3-00	6-67	0-765							
3-30	6-73	0-825							
4-00	6-80	0-895							
4-30	6-82	0-915							
5-00	6-87	0-965	27 secs						
5-30	6-91	1-005							
6-00	6-92	1-015							
6-30	6-99	1-035							
7-00	7-00	1-095							
7-30	7-07	1-165		23.8	420				
8-00	7-10	1-195							
8-30	7-13	1-225							
9-00	7-15	1-245				7.25			
9-30	7-19	1-285							
10-00	7-22	1-315							



Constant Yield Test (Cont) Borehole N<sup>o</sup> NZ 4 (E)

Time (mins)	Water level (metres)	Drawdown (metres)	Yield Sec per 5 gals	Temp °C	Cond µS	pH
00-00	7.23	1.325				
05-00	7.28	1.375	25½			
10-00	7.34	1.435				
15-00	7.37	1.465	26	23.7	420	7.45
20-00	7.42	1.515				
25-00	7.445	1.54				
30-00	7.48	1.575				
35-00	7.50	1.595				
40-00	7.52	1.615				
45-00	7.53	1.625	25	23.8	420	7.25
50-00	7.59	1.685				
55-00	7.61	1.705	25	23.8	420	7.25
00-00	7.65	1.745				
05-00	7.68	1.775	25	23.8	420	7.35
10-00	7.71	1.805	25	23.6	420	7.45
15-00	7.74	1.835	26	23.6	420	7.45
20-00	7.78	1.875	25½	23.6	420	7.45
25-00	7.79	1.885	25	23.6	420	7.45
30-00	7.81	1.905	26	23.6	420	7.45
35-00	7.83	1.925	26	23.6	415	7.45
40-00	7.85	1.945	25	23.6	415	7.50
45-00	7.86	1.955				
Pumping	test stopped at 17-00					

# Recovery Pumping Test

Borehole N° NZ4(A)

Date 27-4-84

Time test started 11-00 pump stopped at 17-00

Pump Cylinder At 19.64 m bgl. Static water rest level before test 5.915 metres

Maximum of water level when pump stopped 7.86 metres below ref point (1.945m)

Ref point - top of pvc casing @ 10 cm s. agl.

Time since pump stopped (mins)	Water level (metres)	S-S' Recovery (metres)	Residual Drawdown (metres)	t/t'	Time since pump stopped (mins)	Water level (metres)	S-S' Recovery (metres)	Residual Drawdown (metres)	t/t'
0-15	7.72	0.14	1.805	1441	20-00	6.55	1.31	0.635	19
0-30	7.68	0.18	1.765	721	25-00	6.51	1.35	0.595	15.4
0-45	7.48	0.38	1.565	481	30-00	6.48	1.38	0.565	13
1-00	7.37	0.49	1.455	361	35-00	6.455	1.405	0.54	11.3
1-30	7.22	0.64	1.305	241	40-00	6.43	1.43	0.515	10
2-00	7.09	0.77	1.175	181	45-00	6.41	1.45	0.495	9
2-30	7.00	0.86	1.085	145	50-00	6.39	1.47	0.475	8.2
3-00	6.94	0.92	1.025	121	55-00	6.375	1.485	0.46	7.5
3-30	6.90	0.96	0.985	103.9	60-00	6.36	1.50	0.4485	7
4-00	6.87	0.99	0.955	91	Measurements stopped at 60 mins (18-00)				
4-30	6.84	1.02	0.925	81					
5-00	6.82	1.04	0.905	73					
5-30	6.78	1.08	0.865	61					
6-00	6.74	1.12	0.825	52.4					
6-30	6.72	1.14	0.805	46					
7-00	6.70	1.16	0.785	41					
8-00	6.68	1.18	0.765	37					
9-00	6.64	1.22	0.725	31					
10-00	6.615	1.245	0.695	26.7					
11-00	6.591	1.269	0.676	23.5					
12-00	6.57	1.29	0.655	21					

Constant Yield Pumping Test.

Borehole N° NZ 413 Village N° 9 INYAMAZURA.

Date 27-4-1984

Time test started 11-00 AM.

Jacob Straight Line Analysis.

$$Q = 54 \text{ L/min.}$$

$$\Delta s_1 = 0.80 \text{ m}$$

$$SWR = 5.915 \text{ metres.}$$

$$\Delta s_2 = 0.53 \text{ m}$$

$$Kb_1 = \frac{2.30 Q}{477.05}$$

$$Kb_1 = \frac{2.30 \times 54 \times 60 \times 24}{1000 \times 477 \times 0.80}$$

$$Kb_2 = \frac{2.30 \times 54 \times 60 \times 24}{1000 \times 477 \times 0.53}$$

$$= 16.38 \text{ m}^3/\text{day/A.}$$

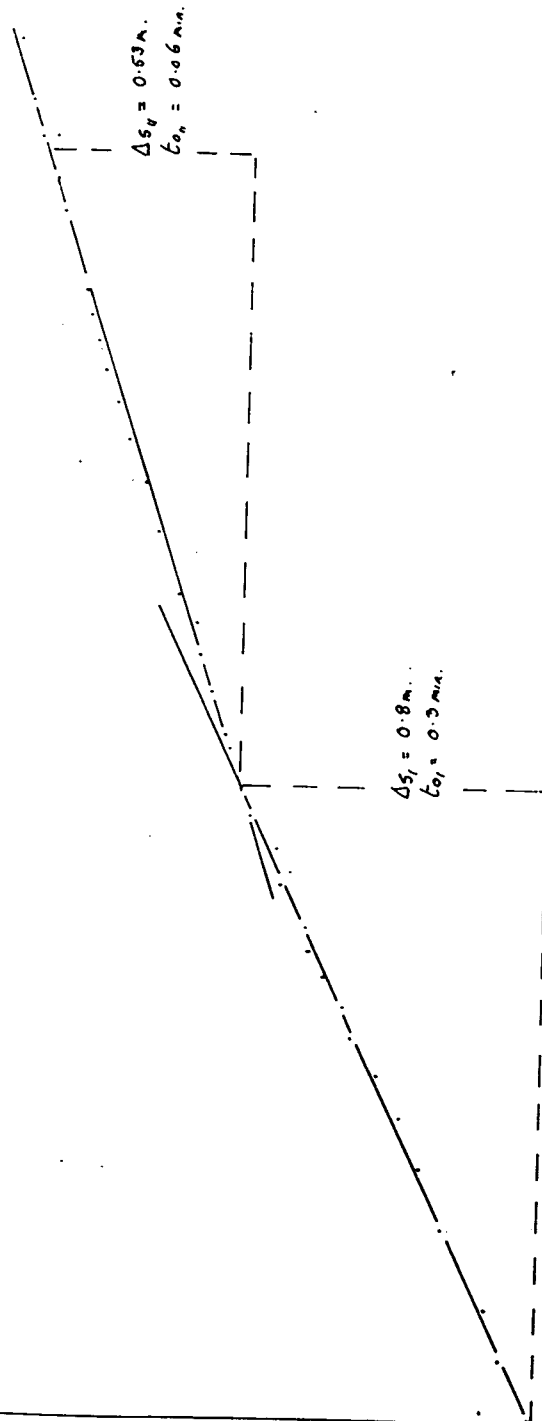
$$= 24.73 \text{ m}^3/\text{day/A.}$$

$\Delta s$   
metres

2

1

0



# Recovery Test.

Bore hole N° NZ 40 VILAGEW' 9 INYAMAZURA.

DATE 27-4-1984

Time started pump 11-00 am. Time stopped pump 1700 hrs

There Recovery effected.

Max  $\Delta s = 7.86m$  below ref level.

SUR 5.9's metres below ref level.

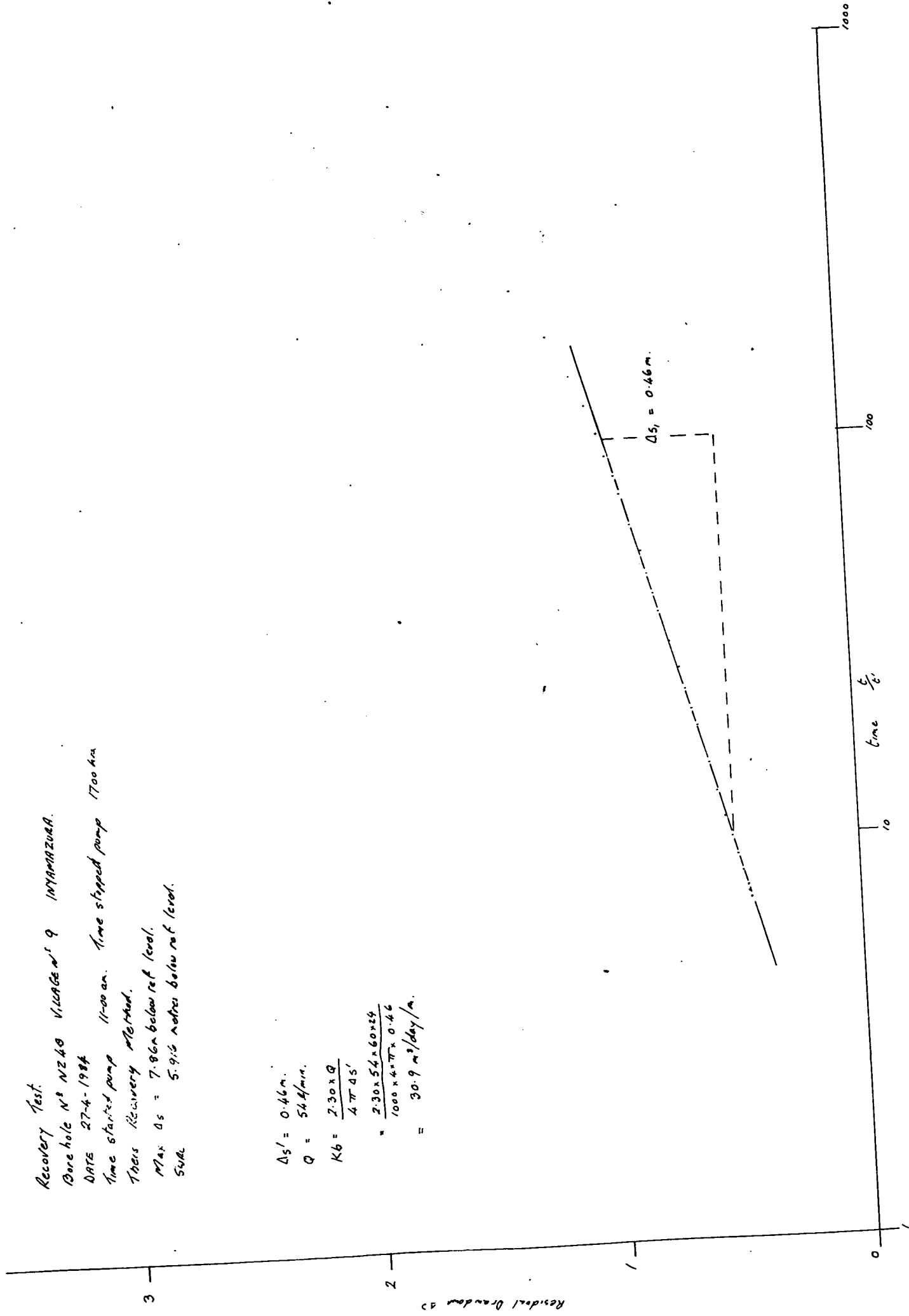
$$\Delta s' = 0.46m.$$

$$Q = 544/min.$$

$$Kb = \frac{2.30 \times Q}{4 \pi \Delta s'}$$

$$= \frac{2.30 \times 544 \times 60 \times 24}{1000 \times 4 \times \pi \times 0.46}$$

$$= 30.9 m^3/day/m.$$



# Constant Yield Pumping Test.

Borehole N<sup>o</sup> NZ 5. VILLAGE 5 IN YAMAZURA.

DATE 2-7-84.

Time Test Started 13-00 hrs.

Pump cylinder ~ <sup>24</sup>~~58~~ metres below ref. point.

Ref point top of casing 0.60 m above ground level.

Pump used - Dando operated single action reciprocating pump.

Time	SWRL (m)					
11-54	3.665 m.	before pump erected.				
12-50	3.965	} water level still recovering after 5 minute yield test to set pump yield.				
12-53	3.920					
12-55	3.89					
12-57	3.88					
Time (mins)	SWL (m)	D.D. (m)	Yield <sup>secs</sup> /5 gal	Temp °C	Cond $\mu$ S.	pH.
00-15	5-52	1.855				
00-30	6.22	2.555				
01-00	7.00	3.335	34.5	24.0	260	7.15
1-15	7.48	3.815				
1-30	8.02	4.355	32	24.0	240	
2-30	8.89	5.225	32	23.8	240	
3-00	9.31	5.645				
3-30	9.62	5.955				
4-00	9.68	6.015				
4-30	9.66	5.995				
5-00	9.73	6.065				
6-00	9.78	6.115				
7-00	9.96	6.245				
8-00	10.46	6.795				
9-00	10.98	7.215				

Constant TIME	Yield Test (Cont) W.C.	D.O.	Borehole YIELD	N <sup>o</sup> NZ5 temp.	Village N <sup>o</sup> 5 Cond.	pH.
10-00	11.56	7.895	32			
12-00	12.30	8.635				
14-00	12.87	9.105				
16-00	13.37	9.605				
18-00	13.76	10.095				
20-00	14.04	10.375				
25-00	14.59	10.825	32	23.8	240	7.25
30-00	15.08	11.315	32			
35-00	15.62	11.955	31			
40-00	16.00	12.335				
45-00	16.46	12.795	32			
50-00	16.76	13.095				
55-00	17.10	13.435	33	24.	230	7.3
60-00	17.25	13.585	32			
74-00	17.80	14.135	32	24	230	7.45
80-00	Dipper could not pass beyond 17.80 metres - pipe socket in the way. Continued to measure yield until that declined and then stabilised - took this to be an indication of a steady state yield?		32			
90-00			32			
100-00			32	24.	230	7.45
110-00			32			
120-00			33			
125-00			34			
130-00			34.5			
135			35.5			
140			35			
145			36			
150			36			
155			36.5			
160			36.75			
				Time (mins)	Yield <sup>secs</sup> /gal.	(Continued)
				165	36.5	
				170	36.5	
				175	36.5	
				180	Test pump stopped	

# Recovery Test

Borehole N<sup>o</sup> NZ5 Village N<sup>o</sup>5 IN YAMAZURA. Date 2-7-84

Borehole diameter 110 mm  $\phi$ . Raising main. 2"  $\phi$  G-I s/s pipe

No water leakage from foot valve

Time pump test started 13-00 hrs

Time pump stopped 16-00 hrs

Pump cylinder at 24 metres below ref point

Static water level before start of test 3.665 metres (b ref point)

Maximum water level when pump stopped 20-22 metres (brp)

Time since pump stopped (mins)	Water level (metres)	Recovery (S-S) (metres)	Residual draw-down (metres)	Time since test started t <sub>1</sub>	Time since pump stopped t <sub>2</sub>
				<del>14.135</del>	72.1
00-15	17-80		14.135	<del>14.135</del>	36.1 72.1
00-30	16-88		13.215	<del>13.215</del>	22.1 36.1
00-45	16-00		12.335	<del>12.335</del>	18.1 24.1
1-00	15-50		11.835	<del>11.835</del>	16.1 18.1
1-15	14-75		11.085	<del>11.085</del>	12.1 14.5
1-30	14-26		10.595	<del>10.595</del>	103.9 12.1
1-45	13-80		10.135	<del>10.135</del>	9.6 103.9
2-00	13-00		9.335	<del>9.335</del>	7.3 9.1
2-30	12-10		8.435	<del>8.435</del>	6.0 7.3
3-00	11-20		7.535	<del>7.535</del>	52.3 6.1
3-30	10-50		6.835	<del>6.835</del>	4.6 52.4
4-00	9-95		6.285	<del>6.285</del>	4.1 4.6
4-30	9-50		5.835	<del>5.835</del>	3.3 4.1
5-00	9-10		5.435	<del>5.435</del>	3.1 3.7
6	8-50		4.835	<del>4.835</del>	26.7 3.1
7	8-11		4.445	<del>4.445</del>	23.5 26.7
8	7-83		4.165	<del>4.165</del>	21. 23.5
9	7-62		3.955	<del>3.955</del>	19. 21.

Recovery Test (contd) B/H N<sup>o</sup> N.25 Village N<sup>o</sup> 5 Date 2-7-84

Time since pump stopped (mins)	Water level (Metres)	Recovery (S-S') (Metres)	Residual Drawdown (Metres)	$\frac{S}{t}$	
10	7.43		3.765	<del>37</del>	19
12	7.16		3.495	<del>36</del>	16
14	6.94		3.275	<del>26.7</del>	13.9
16	6.75		3.085	<del>23.5</del>	12.25
18	6.60		2.935	<del>21</del>	"
20	6.48		2.815	<del>19</del>	10
25	6.22		2.555	<del>15.4</del>	8.2
30	6.04		2.375	<del>13</del>	7
35	5.80		2.135	<del>11.3</del>	6.1
40	5.62		1.955	<del>10</del>	5.5
45	5.50		1.835	<del>9</del>	5
50	5.41		1.745	<del>8.2</del>	4.6
55	5.32		1.655	<del>7.5</del>	4.3
60	5.25		1.585	<del>7.0</del>	4

End of measurements.

$Q = 47.3 \text{ m}^3/\text{day}$

20.22

3.665

16.565



Recovery Test Borehole N° N2 S Village N° 5 INYAMAZURA

Date 2-7-84 This Recovery Method.

Time pump started 13-00

Time pump stopped 16-00

Maximum Drawdown ~ 20-00 metres.

SWR 3.665 metres.

Q = 48 m<sup>3</sup>/day.

$$Kb = \frac{2.30 \times Q}{4\pi \Delta s'}$$

$$\text{for } \Delta s' = 3.4 \text{ m}$$

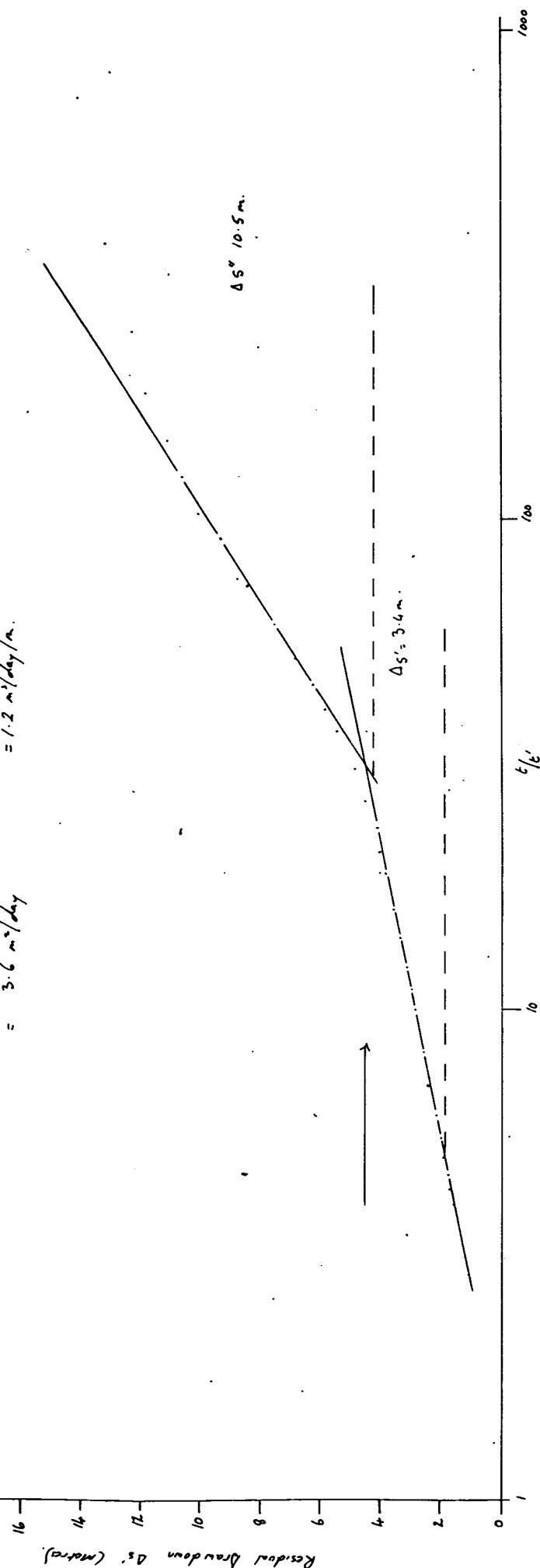
$$Kb = \frac{2.30 \times 48}{4\pi \times 3.4}$$

$$= 3.6 \text{ m}^2/\text{day}$$

$$\text{for } \Delta s'' = 10.5 \text{ m}$$

$$Kb'' = \frac{2.30 \times 48}{4\pi \times 10.5}$$

$$= 1.2 \text{ m}^2/\text{day}$$



Constant Yield Pumping Test    Borehole N° NZ 5    Village N° 5.    INHAMAZURA.  
 Date 2-7-81    Jacob Straight Line Analysis.  
 Static Water Level 3:665 metres.

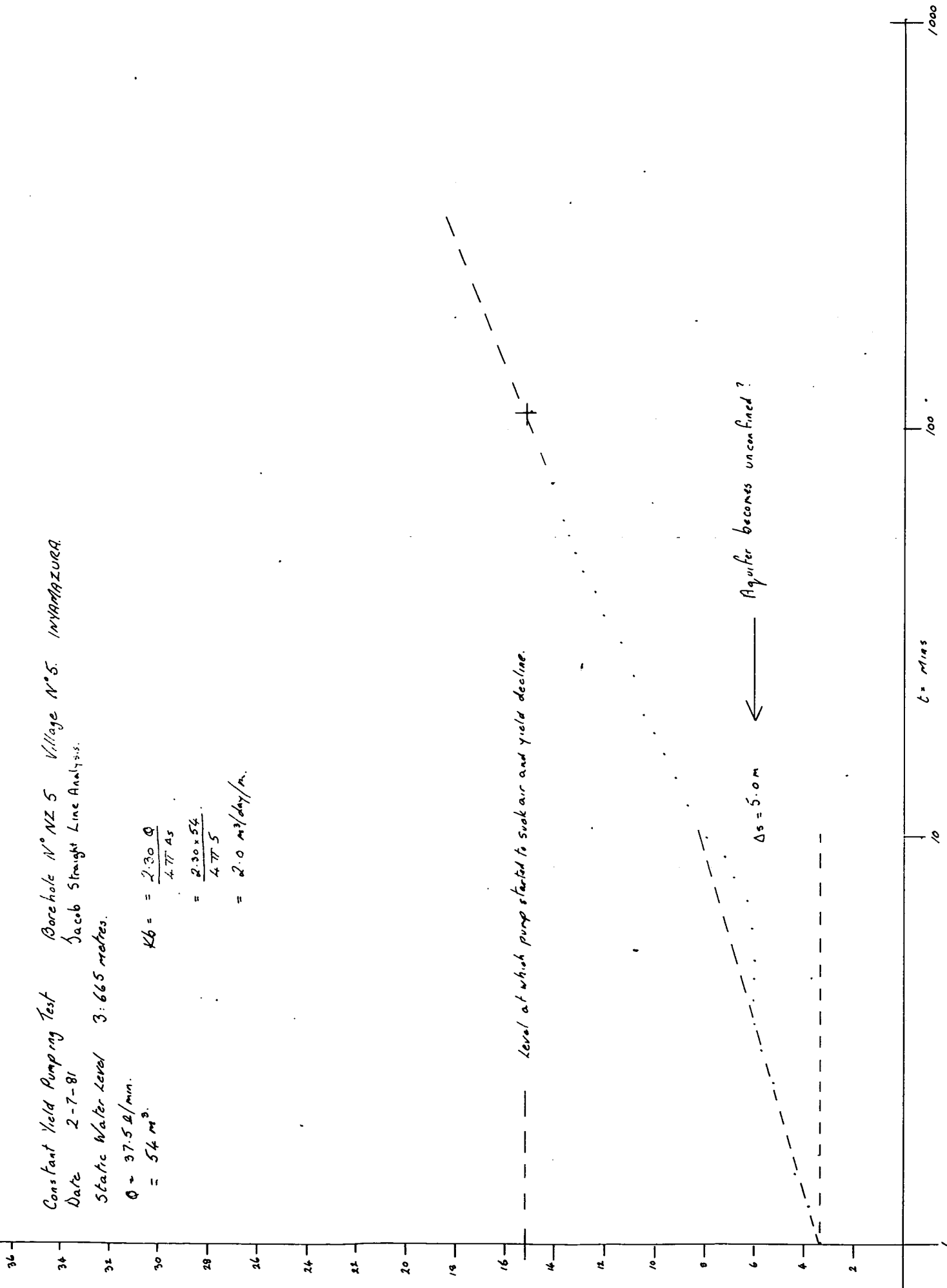
$$Q \approx 37.5 \text{ l/min.}$$

$$= 54 \text{ m}^3.$$

$$Kb = \frac{2.30 Q}{4.77 \Delta s}$$

$$= \frac{2.30 \times 54}{4.775}$$

$$= 2.0 \text{ m}^3/\text{day/m.}$$



# Constant Yield Pumping Test.

Borchile N° NZ6B. Village N° 7 Nyamazura. 2-8-84.

Time Test Started. 11-30 am.

Pump Cylinder Depth. 31-82 metres.

Ref point 0.15 m. a.g.l.

Pump used - Dando operated single action reciprocating pump.

Time Rest Water Level (metres below ref point)

7-00 am. 2.82

11-05 3.07

11-10 3.05

11-15 3.03

11-20 3.02

11-25. 3.00

11-29 2.99.

Time (mins)	Water Level (metres)	Drawdown (metres)	Yield (Secs/20l)	<del>Water</del> Temp. (°C)	Conductivity µs.	pH.
0-15	4-23	1- <del>41</del> 41				
0-30	4-85	2-03				
0-45	5-56	2-74				
1-00	5-95	3-13				
1-15	6-30	3-48				
1-30	6-58	3-76				
1-45	6-76	3-94				
2	6-92	4-10				
2-30	7-12	4-30				
3	7-28	4-46				
3-30	7-50	4-68				
4	7-60	4-78				
4-30	7-70	4-88				

Constant Yield Pumping Test. Borehole N° NZ6B Village N°7 2-8-84 (cont'd).

Time (mins)	Water Level (metres)	Drawdown (metres)	Yield (secs/20.2)	Temp (°C)	Conductivity µS	pH
5	7-80	4-98	32-3	23.2	360	6-65
6	7-96	5-14				
7	8-05	5-23				
8	8-12	5-30				
9	8-19	5-37				
10	8-25	5-43	27-3	23.2	390	7-35
12	8-37	5-55				
14	8-43	5-61				
15	8-46	5-65	27-4	23.2	390	7-45
16	8-48.5	5-66.5				
18	8-54	5-72				
20	8-60	5-78	27-5	23.2	390	7-55
22	8-65.5	5-83.5				
24	8-72	5-90	27-4	23.2	390	7-55
26	8-76	5-94				
28	8-79	5-97				
30	8-84	6-02	27-3	23.2	390	7-55
35	8-94	6-12		23.2		
40	8-99	6-17	26-5	23.2	390	7-60
45	9-03	6-21	27-5	23.2		
50	9-08	6-26	27-3	23.2	400	7.60
55	9-11	6-29	27-5	23.2	390	7.55
60	9-16	6-34	27-1	23.2	400	7.60
70	9-24	6-42	27-5	23.2	390	7-35
80	9-29	6-47	27-5	23.2	410	7-35
90	9-38	6-56	27-5	23.2	380	7-35
100	9-46	6-64	27-0	23.2	400	7-35

Constant Yield Pumping Test. Borehole N<sup>o</sup> NZ6B Village N<sup>o</sup> 7 2-8-84 (cont'd)

Time (mins)	Water Level (metres)	Drawdown (metres)	Yield <del>Secs</del> Secs/20L	Temp (°C)	Conductivity μS	pH
110	9-51	6-69	26-9	23-2	390	7-40
120	9-57.5	6-75.5	27-0	23-2	400	7-45
135	9-63	6-81	27-2	23-2	390	7-30
150	9-70	6-88	27-4	23-2	390	7-40
165	9-76	6-94	27-0	23-2	400	7-45
<del>170</del> 177½	9-78	6-96				
179	9-80	6-98				
180	9-81	6-99	27-3	23-2	400	7-45
HCO <sub>3</sub>	166 ppm					

Time - Drawdown Pumping Test Jacob Straight Line Analysis

Borehole N° NZ 60 Village N° 7 Ayanazura 2-8-84

Static Water Level 2.82 metro below ref level

Test Duration 4 hours - pump stopped after 3 hours

$$Kb = \frac{2.30 \times Q}{4\pi \Delta s}$$

$$Q = 62.84 \text{ m}^3/\text{day} \quad (0.73 \text{ l/sec})$$

$$\Delta s_1 = 2.25 \text{ metros}$$

$$\Delta s_2 = 1.3 \text{ metros}$$

$$Kb_1 = \frac{2.30 \times 62.84}{4\pi \times 2.25}$$

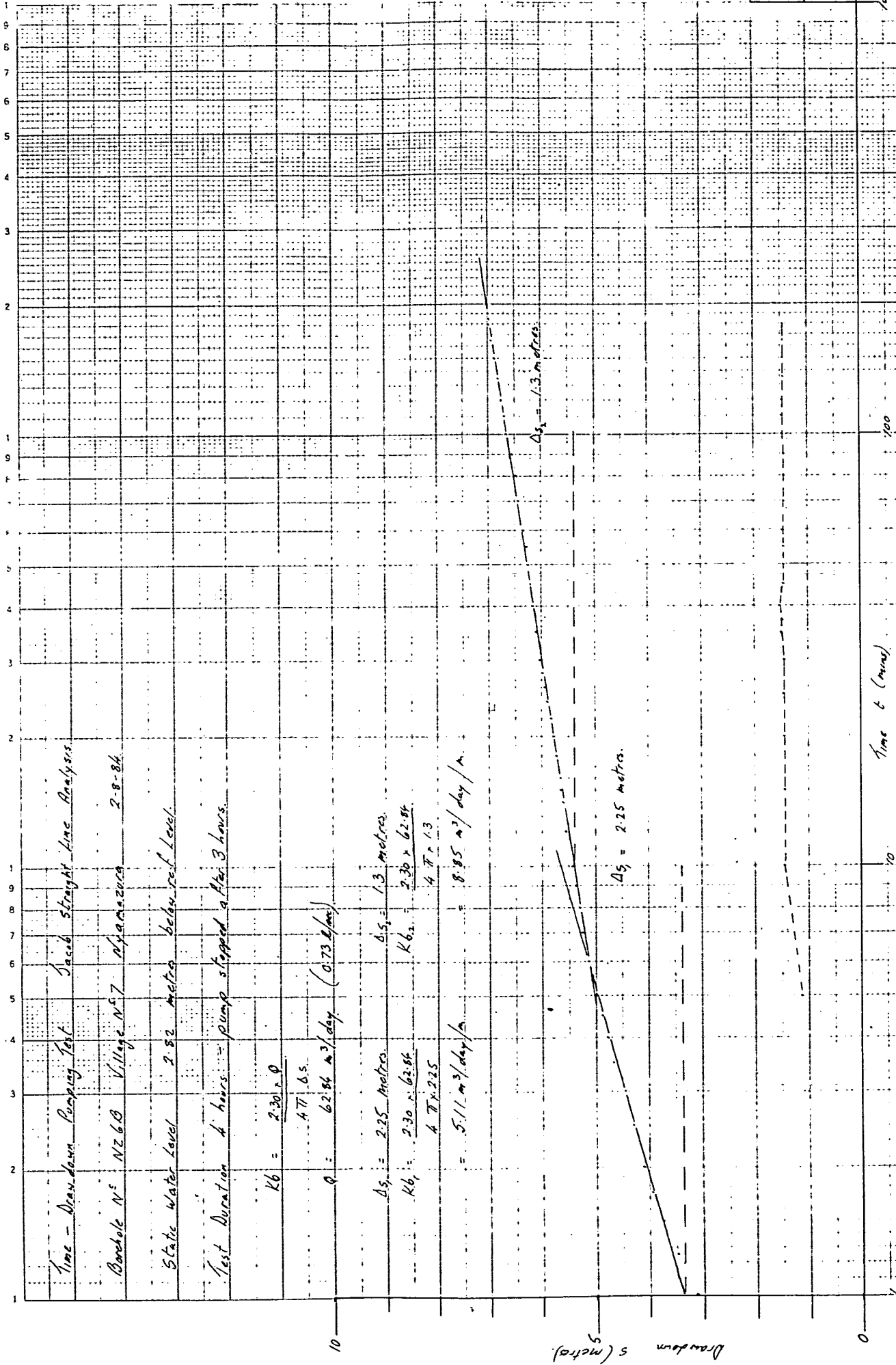
$$Kb_2 = \frac{2.30 \times 62.84}{4\pi \times 1.3}$$

$$= 5.11 \text{ m}^3/\text{day/m}$$

$$= 8.85 \text{ m}^3/\text{day/m}$$

$$\Delta s = 2.25 \text{ metros}$$

$$\Delta s_2 = 1.3 \text{ metros}$$



# Recovery Test

Borehole N° NZ 6 B Village N° 7 Nyamazura 2-8-84

Pump Cylinder Depth 31-82 metres.

Rest Water Level 2.82 metres below ref point.

Ref. Point 0.15 metres above ground level.

Pump used - Dando operated single action reciprocating pump.

Maximum drawdown 6.99 metres

Yield 0.73 l/sec. 62.84 m<sup>3</sup>/day

Time since pump stopped (mins.)	Water Level (metres)	Residual Drawdown (metres)	Recovery (metres)	$\frac{t}{t'}$
0-15	9-09	6-42	0-57	721
0-30	8-40	5-58	1-41	361
0-45	7-80	4-98	2-01	241
0-00	7-23	4-41	2-58	181
0-15	6-70	3-88	3-11	145
0-30	6-17	3-41	3-58	121
0-45	5-77	2-95	4-04	103.9
1-00	5-49	2-57	4-42	91
1-30	5-10	2-28	4-71	73
1-00	4-92	2-10	4-89	61
1-30	4-76	1-96	5-03	52.4
1-45	4-63	1-81	5-13	46
2-00	4-52	1-70	5-29	41
2-15	4-44	1-62	5-37	37
2-30	4-26	1-44	5-55	31
2-45	4-09	1-27	5-72	26.7
3-00	4-00	1-18	5-81	23.5
3-15	3-94.5	1-125	5-865	21
3-30	3-89	1-07	5-92	19

Recovery Test. Borehole N° NZ 6B. Village N° 7 Nyamazura 2-8-84 (cont'd)				
Time since pump stopped. (mins)	Water Level (metres)	Residual Drawdown (metres)	Recovery (metres)	$\frac{t}{t'}$
12	3-815	0-995	5-995	16
14	3-76	0-96	6-03	13-9
16	3-72	0-90	6-09	12-3
18	3-69	0-83	6-16	11
20	3-73	0-91	6-08	10
21	3-745	0-925	6-065	9-6
22	3-725	0-905	6-085	9-2
23	3-695	0-875	6-115	8-8
24	3-67	0-85	6-14	8-5
26	3-62	0-80	6-19	7-9
28	3-585	0-765	6-225	7-4
30	3-55	0-73	6-26	7
35	3-48	0-66	6-33	6-1
40	3-43	0-61	6-38	5-5
45	3-38	0-56	6-43	5
50	3-33	0-51	6-48	4-6
55	3-30	0-48	6-51	4-27
60	3-27	0-45	6-54	4



# Bail Test.

Borehole N° NZ6B Village N° 7 Nyamazura 31-7-84

Rest water level. \ 2-80 metres below ground level.

Capacity of bailer 22 litres

N° of Bails 39.

Time taken 18 mins 17 secs

Drawdown 11-26 metres ( 5-46 metres)

Amount of water bailed 858 litres

Average yield 47.0 l/min ( 0.78 l/sec)

## Recovery

Time after

being stopped

(mins)

	Water Level (metres)	Residual Drawdown (metres)	Recovery (metres)	$\frac{t}{t'}$
5	8-15	5-35	0-11	4-65
10	6-00	3-20	2-26	2-825
15	5-00	2-20	3-26	2-22
20	4-28	1-48	3-98	1-9
25	3-84	1-04	4-42	1-73
30	3-60	0-80	4-66	1-61
35	3-36	0-56	4-90	1-52
40	3-25	0-45	5-01	1-46
45	3-16	0-36	5-10	1-41
50	3-08	0-28	5-18	1-37
55	3-04	0-24	5-22	1-33
60	3-00	0-20	5-26	1-30

$$\Delta S_3'' = 5.6 \text{ metres.}$$

# Constant Yield Pumping Test

Borehole N° NZ 7A, Village N° 6 NYAMAZURA

Date 20-7-84

Time test started 10-30 AM

Pump Cylinder Depth ~ 43 metres

Ref point 10 cms agl

Pump used - Dando operated single action reciprocating pump

Time SWR (metres)

10-19 27-77 Water producing zones: 1-

10-26 27-77 34 - 38 metres

10-29 27-77 40 metres

Hole diameter 204 mm (8")

Time (mins)	Water Level (metres)	Drawdown (metres)	Yield (Secs/2cl.)	Temperature (°C)	Conductivity $\mu$ S	pH
0-15	27-90	0.13				
0-30	27-98	0.21				
0-45	27-09	0.32				
1-00	28- <del>22</del> 22	0.45				
1-15	28-39	0.62				
1-30	28-54	0.77				
1-45	28-67	0.90				
2-00	28-82	1.05				
2-30	29-10	1.33				
2-00	29-51	1.74				
2-30	29-92	2.15				
2-00	30-26	2.49				
2-30	30-69	2.82				
2-00	31-13	3.36				
	32-03	4.26				

Constant Yield Test Borehole N° NZ 7 Village N° 6 NYAMAZURA 20-7-84 (Cont'd)

Time (mins)	Water level (metres)	Drawdown (metres)	Yield (Secs/20L)	Temperature (°C)	Conductivity $\mu S$	pH
7	32-81	5.04				
8	33-31	5.54				
9	33-68	5.91				
10	34-06	6.29				
11	34-55	6.78				
12	35-02	7.25				
14	36-00	8.23				
16	36-82	9.05				
18	38-24	10.47				
20	41-05	13.28				
22	43-43	15.66				
24	43-43	15.66				

Pump started sucking air @ 43-43 after 22 minutes of pumping. Yield dropped dramatically... most of water produced during test was taken directly from storage within the 8" well.

# Recovery Test

Borehole N° NZ 7 Village N° 6. NYAMAZURA.

Date 20-7-84

Time test started - 10-30 hrs.

Time pump stopped 11-30 hrs.

Pump cylinder at ~ 43 metres below gl.

Rest water level. 27-77 metres.

Ref point, 10 cms' agl.

Maximum drawdown experienced. 15-66 metres.

## Yield.

Time since pump stopped (mins)	Water level. (metres)	Residual Drawdown. (metres)	Recovery. (metres)	%
-15				
0-30				
0-45				
1-00	44-45	16-68?	-	
1-15				
1-30	43-25	15-48	0-18	41
1-45	43-22	15-45	0-21	35.3
2-00	43-19	15-42	0-24	31
2-30	43-12	15-35	0-31	25
3-00	43-05	15-28	0-38	21
3-30	42-99	15-22	0-44	18.14
4-00	42-92	15-15	0-51	16
4-30	42-86	15-09	0-57	14.3
5	42-80	15-03	0-63	13
6	42-68	14-91	0-75	11
7	42-56	14-79	0-87	9.57
8	42-44	14-67	0-99	8.5

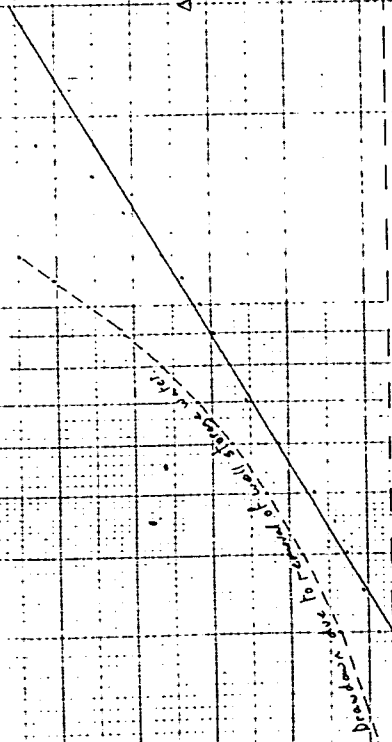
Water running into well →

Recovery Test. Borehole No NZ 7 Village N° 6 NYAMAZURA 20-7-84 (cont'd)

Time since pump stopped. t° (mins)	Water level (metres)	Residual Drawdown. (metres)	Recovery (metres)	t/t°
9	42-32	14-55	1.11	7.7
10	42-20	14-43	1.23	7
12	41-98	14-21	1.45	6
14	41-78	14-01	1.55	5.29
16	41-58	13-81	1.85	4.75
18	41-37	13-60	2.06	4.33
20	41-13	13-36	2.30	4
22	40-95	13-18	2.48	3.73
24	40-75	12-98	2.68	3
26	40-52	12-75	2.81	3.31
28	40-30	12-53	3.13	3.14
30	40-09	12-32	3.34	3
35	39-52	11-75	3.91	2.7
40	38-92	11-15	4.51	2.5
45	38-39	10-62	5.04	2.3
50	37-84	10-07	5.59	2.2
55	37-50	9-73	5.93	2.1
60	37-30	9-53	6.13	2
65	37-09	9-32	6.34	1.92

Time ~~Water~~ Drawdown Pumping Test Jacob Straight Line Analysis  
 Borehole N° 1, Village N° 6 Nyamazauna 20-7-84  
 Static Water level 27.77 metres

Drawdown s (metres)



$$Q = 61.7 \text{ m}^3/\text{day}$$

$$Ks = 9.7 \text{ m}$$

$$Ks = \frac{2.3 \times 61.7}{4\pi \times 9.7}$$

$$= 1.16 \text{ m}^2/\text{day}/\text{m}$$

Time t (min)

# Recovery Test Thesis Analysis

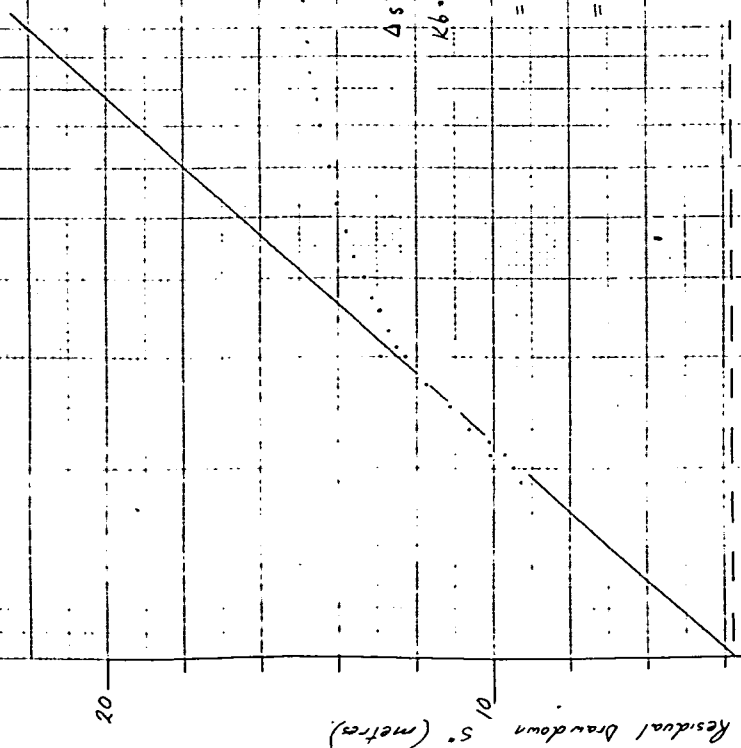
Borehole No NZ7 Village No 6 NYANGAZURA 20-7-84

Static water rest level 27.77m

Max drawdown 15.66m

Yield 4.8 m<sup>3</sup>/day

$$\begin{aligned} \Delta s'' &= 18.2 \text{ m} & Q &= 0.056 \text{ l/sec} \\ & & &= 4.8 \text{ m}^3/\text{day} \\ K &= \frac{2.30 \times Q}{4 \pi \Delta s''} \\ &= \frac{2.30 \times 4.8}{4 \pi \times 18.2} \\ &= 0.048 \text{ m}^3/\text{day/metre} \end{aligned}$$





# Bail Test.

Borehole N<sup>o</sup> N27B. Village N<sup>o</sup> 6. Nyamazura. 10-8-84.

Rest water level. 24.78 metres (bgl)

Capacity of bailer 22 litres.

N<sup>o</sup> of bails 49.

Time taken 30 minutes.

Drawdown. 1.52 metres.

Amount of water bailed. 1.078 m<sup>3</sup>.

Yield. 0.60 l/sec 51.57 m<sup>3</sup>/day.

Specific capacity 33-9.2 m<sup>3</sup>/day / metre of draw down.

Time after bailing stopped. (mins)	Specific capacity Water Level. (metres)	Residual Drawdown. (metres)	Recovery (metres)	t/c".
0-30	26-20	1-42	0-10	61
1-00	26-05	1-27	0-25	31
2	25-86	1-08	0-44	16
4	25-61	0-83	0-69	8.5
6	25-41	0-63	0-89	6
8	25-28	0-50	1-02	4.75
10	25-21	0-43	1-09	4.
15	25-13	0-33	1-19	3.
20	25-06	0-28	1-24	2.5
25	25-02	0-24	1-28	2.2
30	25-00	0-22	1-30	2
35	24-96	0-18	1-34	<del>1.85</del> 1.86.
40	24-95	0-17	1-35	<del>1.75</del> 1.75
45	24-94	0-16	1-36	<del>1.65</del> 1.67
50	24-93	0-15	1-37	1-60
55	24-92	0-14	1-38	1-55
60	24-91	0-13	1-39	1-5.

10

Residual Drawdown. 5' metres.

5

0

Bail test - Recovery Data - Theis analysis  
Borehole N°270 Village N° 6 Njamsara 10-8-84  
Rest water level 24.78 metres  
Maximum drawdown 1.52 metres  
Yield 51.57 m<sup>3</sup>/day  
Duration of test 30 mins

$Kb = 2.30 Q$

$4\pi \Delta s'$

$= 2.30 \times 51.57$

$4\pi \times 0.92$

$= 10.26 \text{ m}^3/\text{day/metre}$

$\Delta s' = 0.92 \text{ metres}$

10

6/6"

100

1000

# Constant Yield Pumping Test

Village N° 3 Inyama zura

Bore hole N° NZ 8

Date: 10-7-84

Cylinder at 33 metres

Q = 57.6 m<sup>3</sup>/day

Yield measured as the number of seconds to fill a 20 litre capacity bucket

Time	Water level	Date
11-29 am	12-11 m	5-7-84
13-25	12-10 m	10-7-84
13-28	12-09 m	10-7-84
13-29	12-095 m	10-7-84

Pumping Test Started at

13-30

Time after pump started (min.)	Water level (metres)	Drawdown (metres)	Yield (Sec/20 litres)	Cond. $\mu$ S	Temp °C	pH
0-15	13-13	1-03	31.6			
0-30	13-47	1-37				
0-45	13-76	1-66				
1-00	13-92	1-82				
1-15	14-02	1-92				
1-30	14-17	2-07				
1-45	14-22	2-12				
2-00	14-33	2-23				
2-30	14-40	2-30				
3-00	14-50	2-40				
3-30	14-59	2-49				
4-00	14-69	2-59				
4-30	14-75	2-65				
5-00	14-80	2-70	29.2	270	23.4	7.35
6	14-92	2-82				
7	14-99	2-89				
8	15-05	2-95				

Constant Time after pump started (min)	Yield Pumping Test Water level (metres)	Drawdown (metres)	Borehole N <sup>o</sup> N28 Yield (Secs/20 litres)	Cond $\mu$ S	Temp $^{\circ}$ C	pH
9	15-11	3-01				
10	15-16	3-06	28.6			
12	15-24	3-14				
14	15-31	3-21	29.5			
16	15-37	3-27				
18	15-43	3-33				
20	15-47	3-37	29.7	265	23.4	7.75
22	15-51	3-41				
24	15-54	3-44	29.6			
26	15-58	3-48				
28	15-61	3-51				
30	15-63	3-53	29.4	265	23.2	7.85
35	15-66	3-56				
40	15-69	3-59				
45	15-77	3-67	29.2	265	23.4	7.70
50	15-82	3-72	<del>30.0</del>	<del>265</del>	<del>23.4</del>	<del>7.85</del>
55	15-84	3-74				
60	15-87	3-77	30.0	265	23.4	7.85
70	15-91	3-81	<del>29.8</del> 29.8	260	23.4	7.90
80	15-98	3-88				
90	16-04	3-94	30.1	255	23.4	8.00
100	16-07	3-97	29.9	255	23.4	8.05
120	16-12	4-02	30.0	255	23.2	8.05
150	16-16	4-06	30.3	255	23.2	8.00
180	16-19	4-09	30.0	255	23.2	7.85
		HCO <sub>3</sub> -	149 ppm			

# Recovery Test

Village N° 3 Inyamazura Borehole N° N2 8

Date 10-7-84.

Cylinder at 33 metres below ground level.

Rest water level. 12-10 metres.

Maximum drawdown of 4-09 metres to 16-19 metres.

Yield 0.67 l/sec. 57.6 m<sup>3</sup>/day.

Time since pump stopped (mins)	Water level (metres)	Residual Drawdown (metres)	Recovery (metres)	t/t'	Time since pump stopped (mins)	Water level (metres)	Residual Drawdown (metres)	Recovery (metres)	t/t'
0-15	15-38	3-28	0-81	721 <del>361</del>	14	12-95	0-85	3-24	<del>247</del> 13.9
0-30	14-83	2-73	1-36	361 <del>241</del>	16	12-9.5	0-815	3-275	<del>255</del> 12.25
0-45	14-45	2-35	1-74	241 <del>181</del>	18	12-875	0-775	3-325	<del>24</del> 11
1-00	14-27	2-17	1-92	181 <del>145</del>	20	12-84	0-74	3-35	<del>24</del> 10
1-15	14-08	1-98	2-11	145 <del>121</del>	22	12-81	0-71	3-38	<del>154</del> 9.2
1-30	13-94	1-84	2-25	121 <del>103.9</del>	24	12-795	0-695	3-405	<del>73</del> 8.5
1-45	13-84	1-74	2-35	103.9 <del>91</del>	26	12-76	0-66	3-43	<del>113</del> 7.9
2-00	13-75	1-65	2-44	91 <del>73</del>	28	12-735	0-635	3-455	<del>14</del> 7.4
2-30	13-62	1-52	2-57	73 <del>61</del>	30	12-715	0-615	3-475	<del>7</del> 7
3-00	13-53	1-43	2-66	61 <del>52.4</del>	35	12-665	0-565	3-535	<del>82</del> 6.1
3-30	13-46	1-36	2-73	52.4 <del>46</del>	40	12-625	0-525	3-575	5.5
4-00	13-40	1-30	2-79	46 <del>41</del>	45	12-59	0-49	3-60	5
4-30	13-36	1-26	2-83	41 <del>37</del>	50	12-56	0-46	3-63	4.6
5-00	13-32	1-22	2-87	37 <del>31</del>	55	12-53	0-43	3-66	4.3
6	13-24	1-14	2-95	31 <del>26.7</del>	60	12-51	0-41	3-68	4
7	13-19	1-09	3-00	26.7 <del>23.5</del>					
8	13-145	1-045	3-045	23.5 <del>21</del>					
9	13-105	1-005	3-085	21 <del>19</del>					
10	13-07	0-97	3-12	19 <del>16</del>					
12	13-005	0-905	3-185	16 <del>7</del>					

# Recovery Test Borehole N° NZ 8 Village N° 3 Izamazura.

Date 10-7-84 This Recovery Method.

Time pump started 13-30

Time pump stopped. 16-30

Maximum Drawdown. 4-09 metres.

Swirl 12-10 metres.

Q = 57.6 m³/day.

$$Kb = \frac{2.30 \times Q}{4\pi \Delta s}$$

for  $\Delta s' = 0.85m$ .

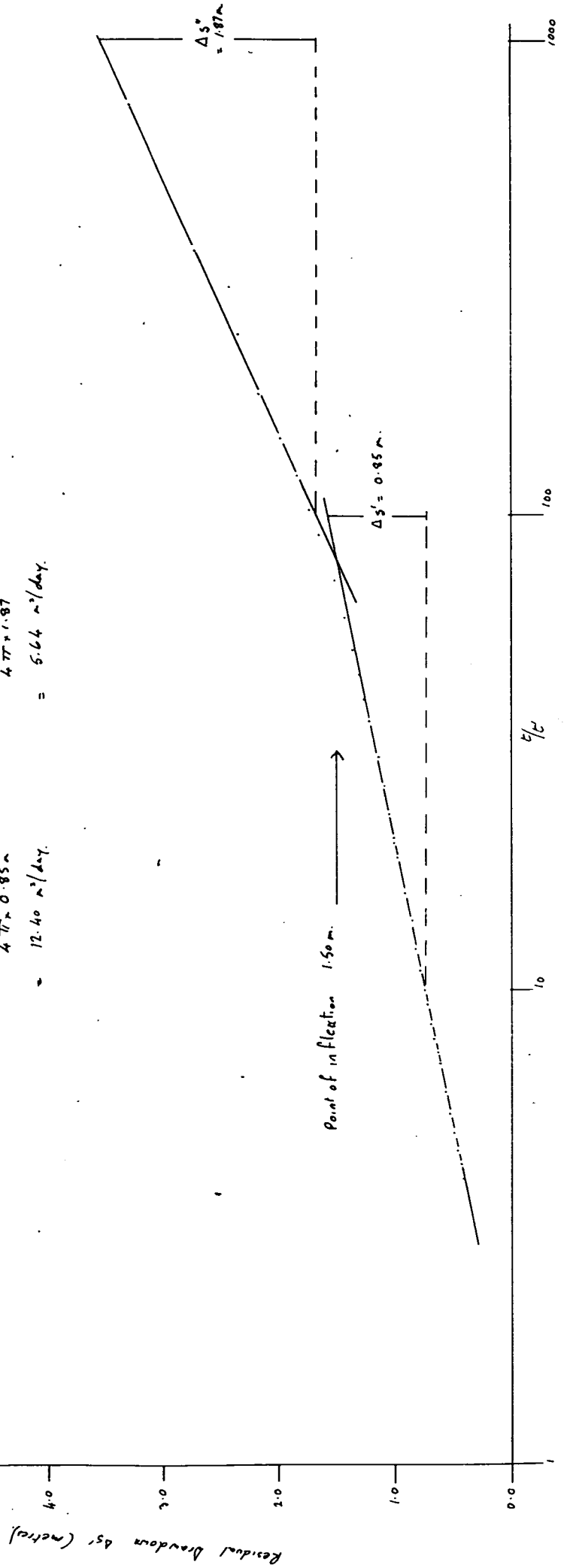
$$Kb' = \frac{2.30 \times 57.6}{4\pi \times 0.85}$$

$$= 12.40 \text{ m}^3/\text{day}.$$

for  $\Delta s'' = 1.87m$ .

$$Kb'' = \frac{2.3 \times 57.6}{4\pi \times 1.87}$$

$$= 5.64 \text{ m}^3/\text{day}.$$



Constant Yield Pumping Test. Borehole N° 28 Village N° 3 Inyanga.

Date 10-7-84 Jacob Straight Line Analysis.

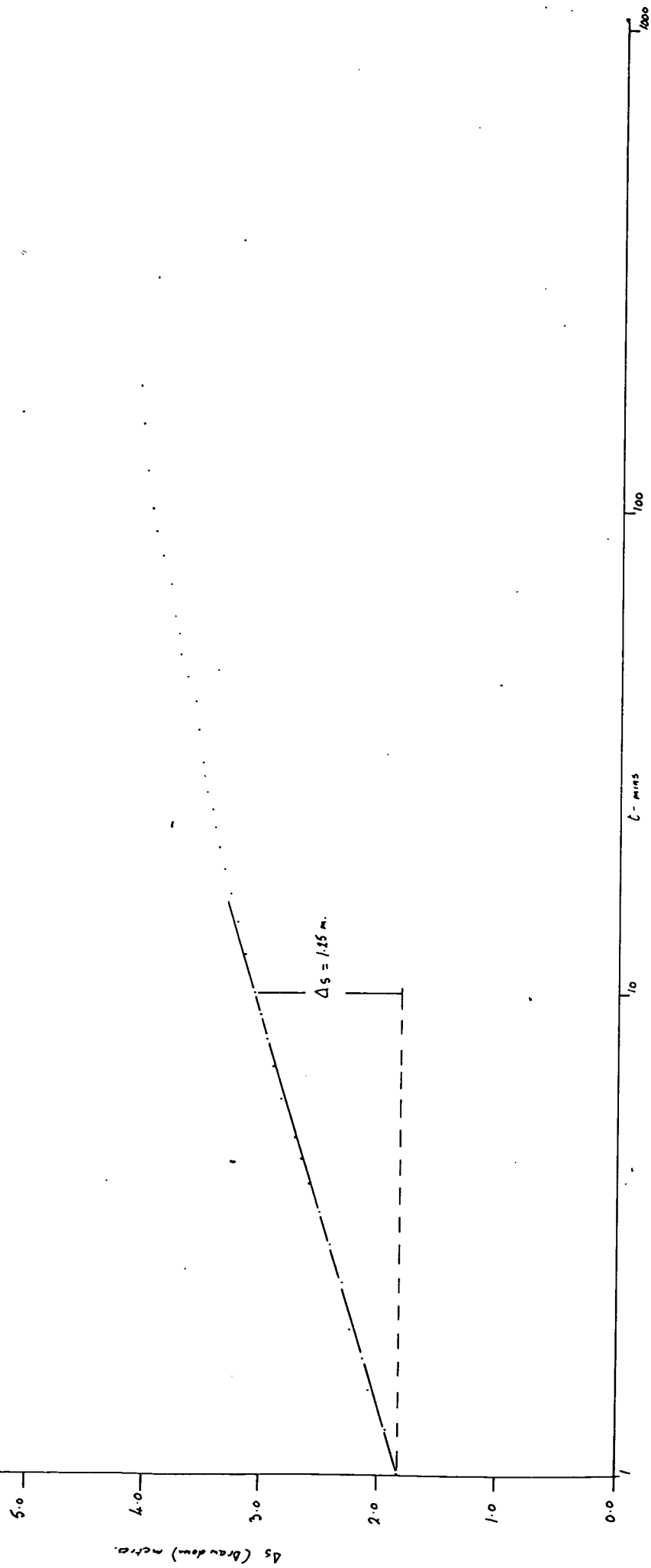
Static Water Level 12.10 metres.

$Q = 57.6 \text{ m}^3/\text{day}.$

$$Kb = \frac{230 Q}{4 \pi \Delta s}$$

$$= \frac{230 \times 57.6}{4 \pi \times 1.25}$$

$$= 8.43$$



# Constant Yield Pumping Test.

Borehole N° NZ 9 Village N° 1 A Inyamazura. 18-7-84.

Time test started 13-00 hrs.

Pump cylinder 28.50 metres below ground level.

Ref point ~ 30 cms a.g.l.

Pump used - Dando operated single action reciprocating pump.

Time SWRL (m.)

12-42 16-09

12-44 16-10

Hole depth 30.80 metres.

12-49 16-09

12-52 16-09

12-55 16-09

12-58 16-09

Time (mins)	Water level. (metres).	Drawdown. (metres)	Yield. (lts/20 s)	Temp (°C)	Conductivity µS	pH.
0-15	16-86	0-77				
0-30	17-15	1-06				
0-45	17-31	1-22				
1	17-41	1-32	29.7	24.2	340	7.8
1-15	17-45	1-36				
1-30	17-50	1-41				
1-45	17-53	1-46				
2	17-63	1-54				
2-30	17-64	1-55				
3	17-70	1-61				
3-30	17-74	1-65				
4	17-78	1-69				
4-30	17-86	1-75				
5	17-94	1-77	29.0	24.2	340	8.00
6	17-97	1-85				



Constant Yield Pumping Test.			N 2 9	18-7-84 (Cont'd)		
Time (mins)	Water level (metres)	Drawdown (metres)	Yield (Secs/20 l)	Temp °C.	Conductivity µs.	pH.
7	17-97	1.88				
8	18-05	1.915				
9	18-045	1.955				
10	18-065	1.975	28.5	24.0	335	8.05
12	18-115	2.025				
14	18-16	2.07	28.5	24.0	335	8.05
16	18-187	2.097				
18	18-205	2.115				
20	18-23	2.14	28.5	24.0	335	8.05
22	18-25	2.16				
24	18-27	2.17	28.6	24.0	330	8.05
26	18-28	2.19				
28	18-29	2.20				
30	18-302	2.21	28.6	24.0	330	8.05
35	18-345	2.255	28.6	24.0	330	8.05
40	18-37	2.28	28.6	24.0	335	8.10
45	18-39	2.30	28.5	24.0	325	8.05
50	18-405	2.315	28.6	24.2	325	8.05
55	18-42	2.33	28.6	24.0	330	8.05
60	18-432	2.342	28.6	24.0	325	8.05
65	18-45	2.36				
70	18-45	2.36	28.5	24.0	325	8.05
75	18-46	2.37				
80	18-48	2.39	28.6	24.0	320	8.00
85	18-465	2.375				
90	18-46	2.37	28.6	23.8	320	7.70

Constant Yield Pumping Test. N29. 18-7-84 (cont'd)

Time (mins)	Water level (metres)	Drawdown (metres)	Yield (Secs/200)	Temp °C.	Conductivity µs.	pH.
100	18.49	2.40	28.4	23.8	320	7.70
110	18.51	2.42	28.8	24.0	320	7.75
115	18.51	2.42				
120	18.511	2.421	28.7	<del>24.0</del> 24.0	320	7.75
140	18.54	2.45 (130)	28.7	24.0	320	7.75
		(150)	28.6 28.5	24.0 24.2	320 315	7.80 7.85
160	18.545	2.455	28.5	24.0	320	7.80
177	18.565	2.475 (170)	28.4	24.2	315	7.85
180	18.570	2.48	28.5	24.2	315	7.85

●  $\text{HCO}_3^-$  - 200 ppm @ 160 mins.

# Recovery Test.

Bore hole N° N2 9 Village N° 1A Inyanazura. 18-7-84.

Pump cylinder at 28°50 m. below ground level.

Rest water level. 16-09 metres. (below ref point)

Ref point 30 cms. above ground level.

Maximum draw down. 2.48 metres.

Yield. 0.699 l/sec

60.4 m<sup>3</sup>/day

Time since pump stopped. (mins)	Water Level (metres)	Residual Drawdown. (metres)	Recovery (metres)	$\frac{t}{t_1}$	
0-15	18-18	2-09	0-39	<del>72</del>	721
0-30	17-95	1-86	0-62	<del>36</del>	361
0-45	17-72	1-63	0-85	<del>24</del>	241
	17-49	1-40	1-08	<del>18</del>	181
0-15	17-43	1-34	1-14	<del>12</del>	145
0-30	17-32	1-23	1-25	<del>10</del>	121
0-45	17-16	1-07	1-41	<del>9</del>	103.9
2	17-05	0-96	1-52	<del>7</del>	91
2-30	16-89	0-80	1-68	<del>6</del>	73
3	16-76	0-67	1-81	<del>5</del>	61
3-30	16-64	0-55	1-93	<del>4</del>	52.4
4	16-57	0-48	2-00	<del>3</del>	46
4-30	16-52	0-43	2-05	<del>3</del>	41
5	16-48	0-39	2-09	<del>3</del>	37
6	16-42	0-33	2-16	<del>2</del>	31
7	16-33	0-293	2-287	<del>2</del>	26.7
8	16-36	0-27	2-21	<del>2</del>	23.5
9	16-34	0-25	2-23	<del>1</del>	21
10	16-328	0-238	2-242	<del>1</del>	19
12	16-305	0-215	2-265		16

Recovery time since pump stopped. (mins)	Test. NZ 9 Water level. (metres)	Village N° 1A Residual Drawdown. (metres)	18-7-84 Recovery (metres)	(cont'd) t/t.
14	16-29	0-20	2-28	<del>13.9</del> 13.9
16	16-278	0-188	2-292	12.25
18	16-27	0-18	2-30	11
20	16-26	0-17	2-31	10
22	16-25	0-16	2-32	9.2
24	16-245	0-155	2-325	8.5
26	16-239	0-149	2-331	7.9
28	16-23	0-14	2-34	7.4
30	16-225	0-135	2-345	7
35	16-214	0-124	2-354	6.1
40	16-204	0-114	2-364	5.5
45	16-20	0-11	2-37	5
50	16-19	0-10	2-38	4.6
55	16-184	0-094	2-384	4.27
60	16-18	0-09	2-39	4

Recovery Test - Thesis Analysis.  
 Borehole N° N29 Village 1B. Inyamazuro. 18/7/84.

Static water level 16.09 metres

$Q = 60.4 \text{ m}^3/\text{day}$

Maximum draw down = 2.48 metres

$$Kb = \frac{2.30 \times Q}{4 \pi \Delta s'}$$

$$\text{for } \Delta s'_1 = 0.25 \text{ metres}$$

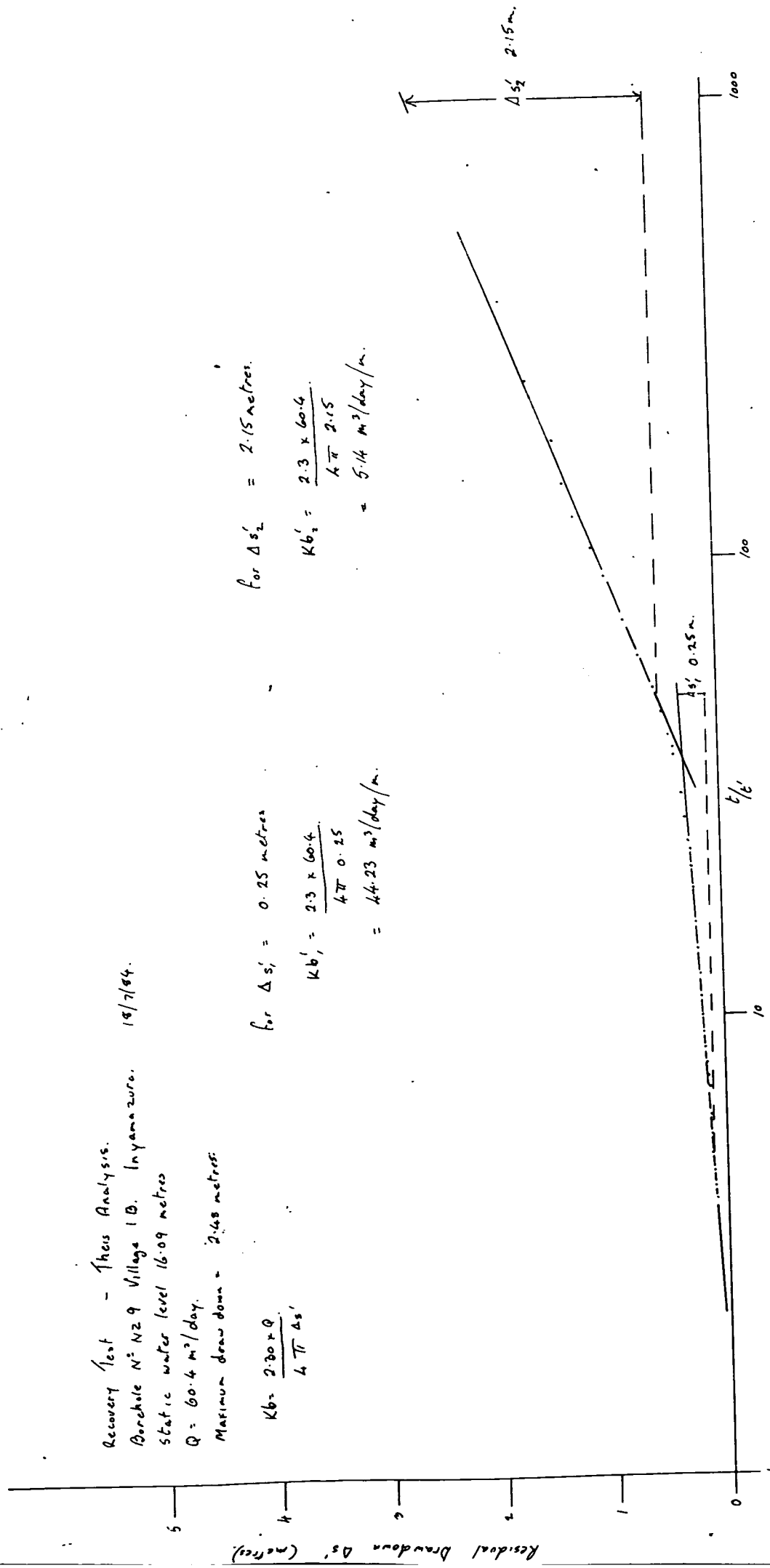
$$Kb'_1 = \frac{2.3 \times 60.4}{4 \pi \times 0.25}$$

$$= 44.23 \text{ m}^3/\text{day/m.}$$

$$\text{for } \Delta s'_2 = 2.15 \text{ metres.}$$

$$Kb'_2 = \frac{2.3 \times 60.4}{4 \pi \times 2.15}$$

$$= 5.14 \text{ m}^3/\text{day/m.}$$



Yield-Drawdown Test. Jacob Straight Line Analysis.  
 Borehole N° N29 Village N° 1A. Irayanzura 18-7-94  
 Static Water Level = 16.09 metres.  
 $Q = 60.4 \text{ m}^3/\text{day}$ .

$$Kb = \frac{2.30 Q}{4 \pi \Delta s_1}$$

$$\text{for } \Delta s_1 = 0.67 \text{ m}$$

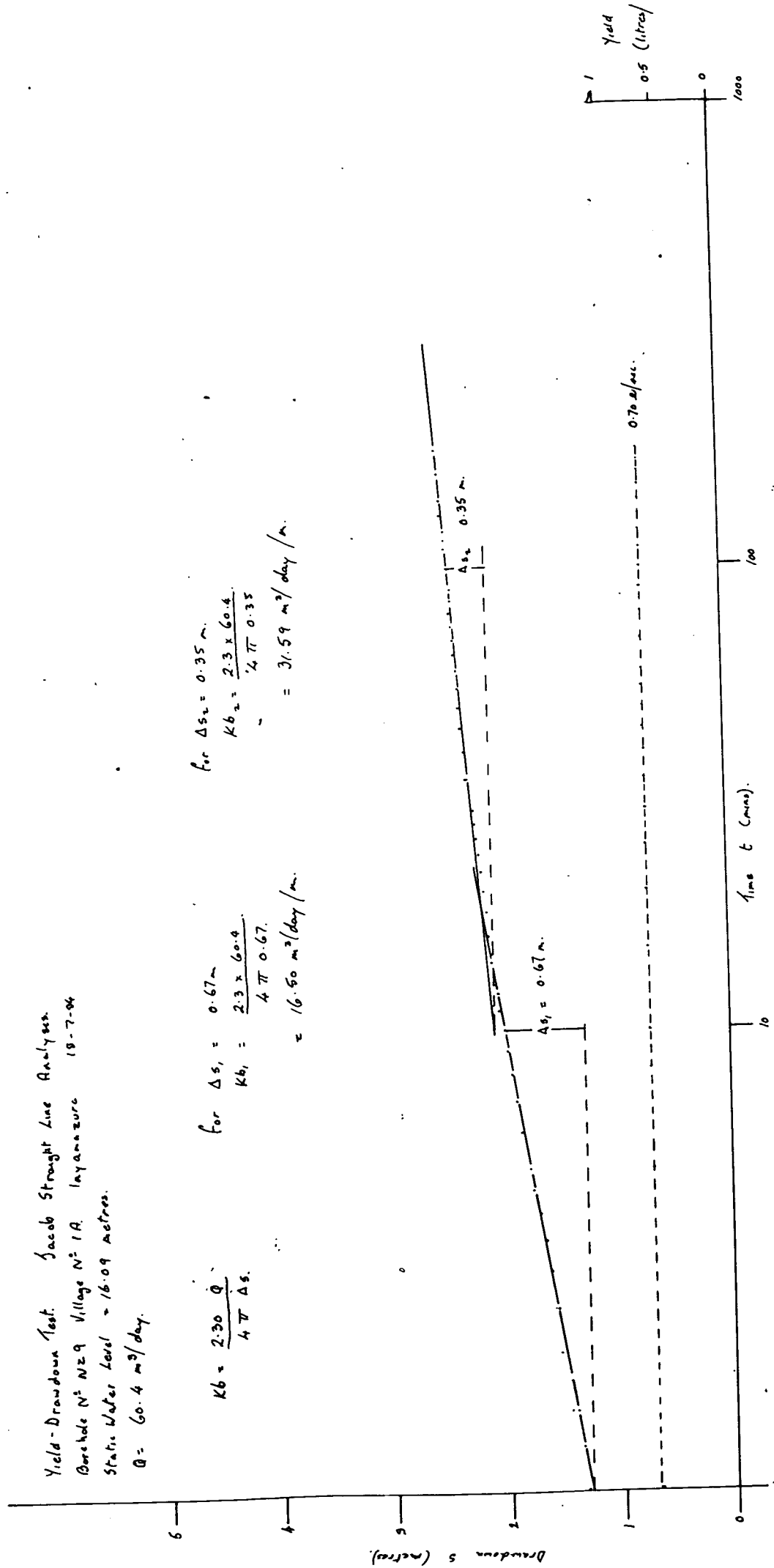
$$Kb_1 = \frac{2.3 \times 60.4}{4 \pi \times 0.67}$$

$$= 16.50 \text{ m}^3/\text{day/m}$$

$$\text{for } \Delta s_2 = 0.35 \text{ m}$$

$$Kb_2 = \frac{2.3 \times 60.4}{4 \pi \times 0.35}$$

$$= 31.59 \text{ m}^3/\text{day/m}$$



# Constant Yield Pumping Test.

Village N° 4 IN YAMAZURA.

Borehole N° NZ 10.

Date 11-7-84.

Cylinder at 25.5 metres below ground level.

Yield measured in number of seconds to fill a 20 litre capacity bucket.

Time Water level.  $Q = 49.25 \text{ m}^3/\text{day}$

14-11 6.88 metres

14-14 6.88 metres

Pumping test started at 14-15.

Time after pump started (mins)	Water level (metres)	Drawdown (metres)	Yield (secs/200)	Cond $\mu\text{S}$	Temp $^{\circ}\text{C}$	pH
15	7-74	0-86				
30	8-07	1-19				
45	8-31	1-43				
1-00	8-39	1-51				
1-15	8-50	1-62				
1-30	8-54	1-66				
1-45	8-60	1-72				
2-00	8-65	1-77				
2-30	8-73	1-85	33.9			
3-00	8-76	1-88				
3-30	8-79	1-91				
4-00	8-82.5	1-94.5				
4-30	8-86	1-98				
5	8-88	2-00	33.6			
6	8-90.5	2-02.5				
7	8-93	2-05				
8	8-96	2-08				
9	8-97	2-09				

Constant	Yield Test.	NZ10 Cont'd	Yield.	Cond $\mu S$	Temp $^{\circ}C$	pH
Time after pump started (mins)	Water level (metres)	Drawdown (metres)	(Secs/20L)			
10	8-99	2-11	33.2	410	22.6	7.45
12	9-025	2-145	<del>33.2</del>	<del>410</del>	<del>22.6</del>	<del>7.45</del>
14	9-05	2-17	34.0			
16	9-07	2-19				
18	9-085	2-205				
20	9-09	2-21	33.9	390	22.6	7.95
25	9-125	2-245	34.1			
30	9-15	2-27	34.2	400	22.6	8.05
35	9-165	2-285	34.4			
40	9-19	2-31	34.4	400	22.6	8.10
45	9-21	2-33	34.2			
50	9-20	2-32	34.2	400	22.4	8.20
55	9-23	2-35	34.2			
60	9-23	2-35	34.2	400	22.4	8.20
70	9-22	2-34	34.6	395	22.4	8.25
80	9-245	2-365	34.4	395	22.2	8.45
90	9-265	2-385	34.4	395	22.2	8.50
100	9-275	2-395	34.4	395	22.2	8.50
110	9-29	2-41	34.5	390	22.0	8.50
120	9-30	2-42	34.5	390	22.0	8.45
150	9-35	2-47	34.6	390	22.2	8.35
180	9-375	2-495	34.5	390	22.2	8.40

$HCO_3^- = 217 \text{ ppm}$



# Recovery Test.

Village N° 4. Inyamazura.

Borehole N° NZ 10.

Date. 11-7-84.

Cylinder at 25.5 metres below ground level.

Rest water level 6.88 metres.

Maximum draw down 2.495 metres to 9.375 metres.

Yield. 0.57 l/sec. 49.25 m<sup>3</sup>/day.

Time since pump stopped (mins).	Water level (Metres)	Residual Drawdown (Metres)	Recovery (Metres)	t/t <sub>0</sub>
0-15	8-60	1-72	0.775	<del>72</del> 72
0-30	8-10	1-22	1.275	<del>36</del> 36
0-45	7-83	0-95	1.545	<del>24</del> 24
1-00	7-66	0-78	1.715	<del>18</del> 18
1-15	7-56	0-68	1.815	<del>14.5</del> 14.5
1-30	7-49	0-61	1.885	<del>12</del> 12
1-45	7-44	0-56	1.935	<del>10.3</del> 10.3
2-00	7-40.5	0-52.5	1.970	<del>9.1</del> 9.1
2-30	7-36	0-48	2.015	<del>7.3</del> 7.3
3-00	7-33	0-45	2.045	<del>6.1</del> 6.1
3-30	7-31	0-43	2.065	<del>5.2</del> 5.2
4-00	7-29	0-41	2.085	<del>4.6</del> 4.6
4-30	7-27.5	0-39.5	2.100	<del>4.1</del> 4.1
5-00	7-26	0-38	2.115	<del>3.7</del> 3.7
6	7-24	0-36	2.135	<del>3.1</del> 3.1
7	7-22	0-34	2.155	<del>2.6</del> 2.6
8	7-21	0-33	2.165	<del>2.3</del> 2.3
9	7-19.5	0-31.5	2.180	<del>2.1</del> 2.1
10	7-19	0-31	2.185	<del>1.9</del> 1.9
12	7-17	0-29	2.205	<del>1.6</del> 1.6

Recovery Test	Borehole N <sup>o</sup> . NZ10. ( <del>cont</del> Cont'd)			
Time since pump stopped.	Water level.	Residual Drawdown	Recovery	c/t.
(mins.)	(metres).	(metres).		
14	7.156	0-276	2.219	<del>26.7</del> 13.9
16	7.143	0-263	2.232	<del>23.5</del> 12.25
18	7.135	0-255	2.240	<del>21</del> 11
20	7.127	0-247	2.248	<del>19</del> 10
25	7.11	0-23	2.265	<del>18.4</del> 9.2
30	7.10	0-22	2.275	<del>18</del> 7
35	7.09	0-21	2.285	<del>17.5</del> 6.1
40	7.08	0-20	2.295	<del>16</del> 5.5
45	7.07	0-19	2.305	<del>15</del> 5
50	7.06	0-18	2.315	<del>14.5</del> 4.6
55	7.06	0-18	2.315	<del>14</del> 4.3
60	7.055	0-175	2.320	<del>13.5</del> 4

Constant Yield Pumping Test Borehole N° 10 Village N° 4 Inyanazura.  
 Date 11-7-84 Jacob Straight Line Analysis.  
 Static Water Level 6.88 metres.

$$Q = 49.25 \text{ m}^3/\text{day}.$$

$$Kb = \frac{230 Q}{4 \pi \Delta s}$$

$$\Delta s' = 0.65 \text{ m.}$$

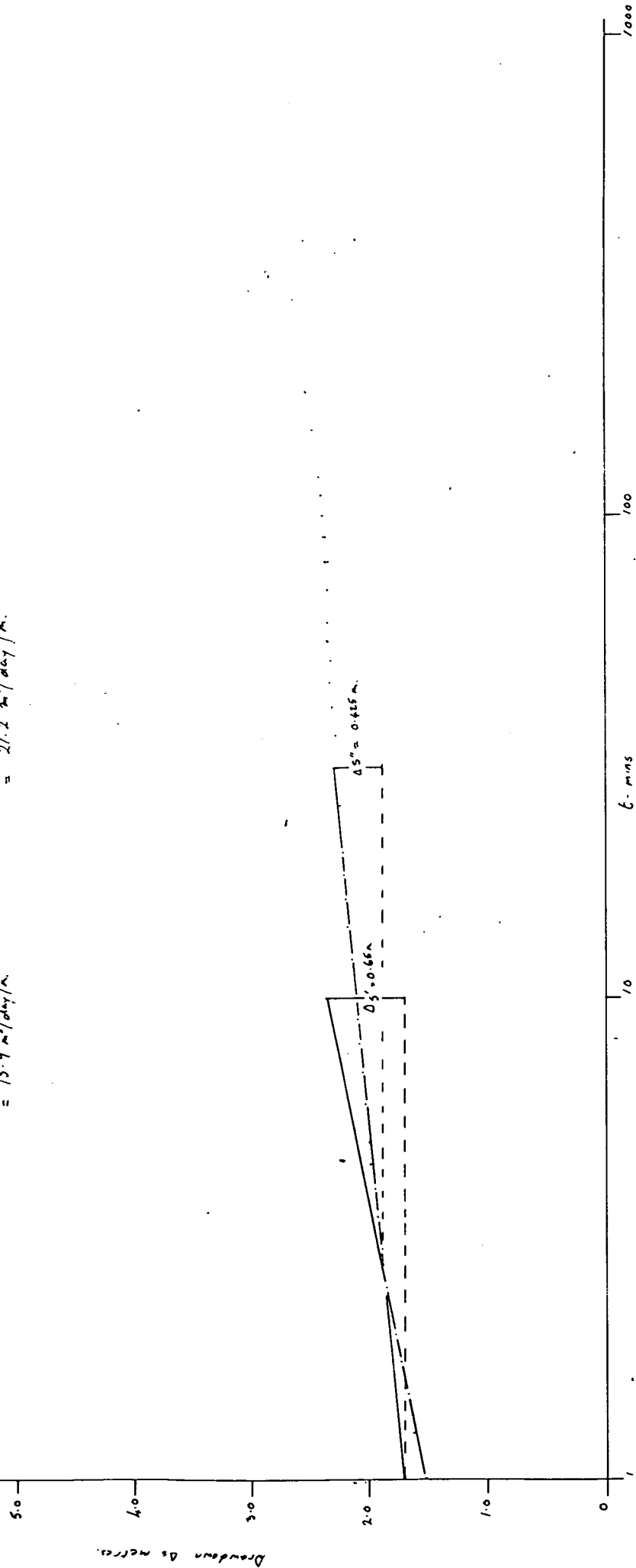
$$Kb' = \frac{230 \times 49.25}{4 \pi \times 0.65}$$

$$= 13.9 \text{ m}^3/\text{day/m.}$$

$$\Delta s'' = 0.425 \text{ m.}$$

$$Kb'' = \frac{230 \times 49.25}{4 \pi \times 0.425}$$

$$= 21.2 \text{ m}^3/\text{day/m.}$$



Recovery Test      Borehole N° 10      Village N° 4      Inyamazura.  
 Date 11-7-84      Their Recovery Method.

Time pump started 16-15

Time pump stopped 17-15

Maximum Drawdown 2.495 metres.

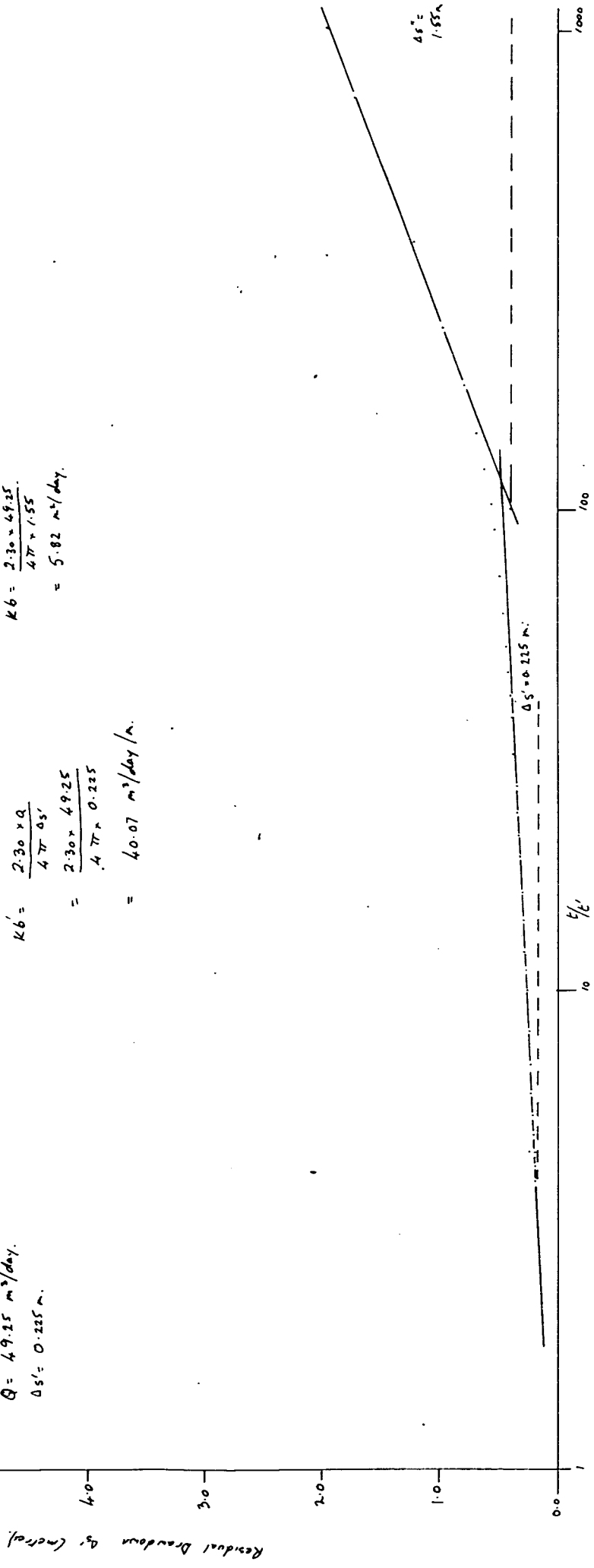
Static Water Rest Level 6.88 metres.

$Q = 49.25 \text{ m}^3/\text{day}.$

$s_s' = 0.225 \text{ m}.$

$$\begin{aligned} \text{For } s_s' &= 1.55 \text{ m} \\ Kb &= \frac{2.30 \times 49.25}{4\pi \times 1.55} \\ &= 5.82 \text{ m}^2/\text{day}. \end{aligned}$$

$$\begin{aligned} Kb' &= \frac{2.30 \times Q}{4\pi s_s'} \\ &= \frac{2.30 \times 49.25}{4\pi \times 0.225} \\ &= 40.07 \text{ m}^2/\text{day/m}. \end{aligned}$$



# Constant Yield Pumping Test

Borehole N° NZ 11A Village N° 2 INYAMAZURA

Date 16-7-84

Time test started 15-00 hrs

Pump Cylinder 24.62 metres below ground level

Dipper would not pass beyond 23.72 metres - top of the cylinder

Ref point 0.50 cmr agl

Pump used - Dando operated single action reciprocating pump

Time SWRL (m)

14-18 4-17

14-43 4-17

14-49 4-17

Time (mins)	Water level (metres)	Drawdown (metres)	Yield (secs/20 litres)	Temp °C	Conductivity µS	pH
0-15	6-00	1-83	24	23.8	340	7.7
0-30	6-93	2-76				
0-45	7- <del>83</del> 62	3-45				
1	8-33	4-16				
1-15	8-97	4-80				
1-30	9-50	5-33				
1-45	9-96	5-89				
2	10-24	6-07				
2-30	11-04	6-87				
3	11-82	7-65				
3-30	12-37	8-20				
4	12-97	8-80				
4-30	13-32	9-15				
5	13-66	9-45	29	23.0		

Constant Yield Test N211 16/1/84 cont'd

Time (mins.)	Water level (metres)	Drawdown (metres)	Yield (Secs/20 litres)	Temp (°C)	Conductivity (µs)	pH
5-30						
6	14-49	10-32				
6-30						
7	15-31	11-14				
8	16-10	11-93				
9	17-08	13-91				
10	18-50	14-33	34	22.8	330	7.9
12	18-64	14-47				
13	19-21	15-04				
14	20-02	15-85				
15			15 35	22.6	300	8.05
16	20-83	16-66				
18	21-05	16-88				
20	21-48	17-31	36	22.6	300	8.4
22	22-77	18-60				
24	23-35	19-16				
<del>25</del> 25	23-72	19-55	35.4	22.6	310	8.4
<del>27</del> 30			34.8			
<del>28</del> 35			55			
<del>30</del> 40			59.8	22.6	325	8.2
<del>35</del> 45			62.5			
<del>40</del> 50			62.6	22.4	325	8.67
<del>45</del> 55			62.6	22.6	330	8.70
60			62.6	22.6	330	8.701
65			64.7	22.6	330	8.75
75			65.5	22.6	343	8.85
80			65.8	22.6	330	8.95
85			68.0	22.6	330	8.95
95			68.6	22.6	330	8.94

Constant Yield Test NZ11 16/7/84 (cont'd)

Depth (m)	Water level (metres)	Drawdown (metres)	Yield (Sax/20 litres)	Temp (°C)	Conductivity (µs)	pH
100			71	22.6	340	8.98
105			71.6	22.6	330	8.85
110			73.0	22.6	330	8.85
115			74.5	22.6	330	8.85

# Recovery Test.

Borehole N<sup>o</sup> 1 NZ 11 Village N<sup>o</sup> 2 Inyamasura.

Date 16-7-84.

Pump cylinder at 24.62 metres below ground level.

Rest Water level 4.17 metres (below ref. point)

Ref. point 50 cm. above ground level.

Maximum draw-down. — about 20-23 metres.

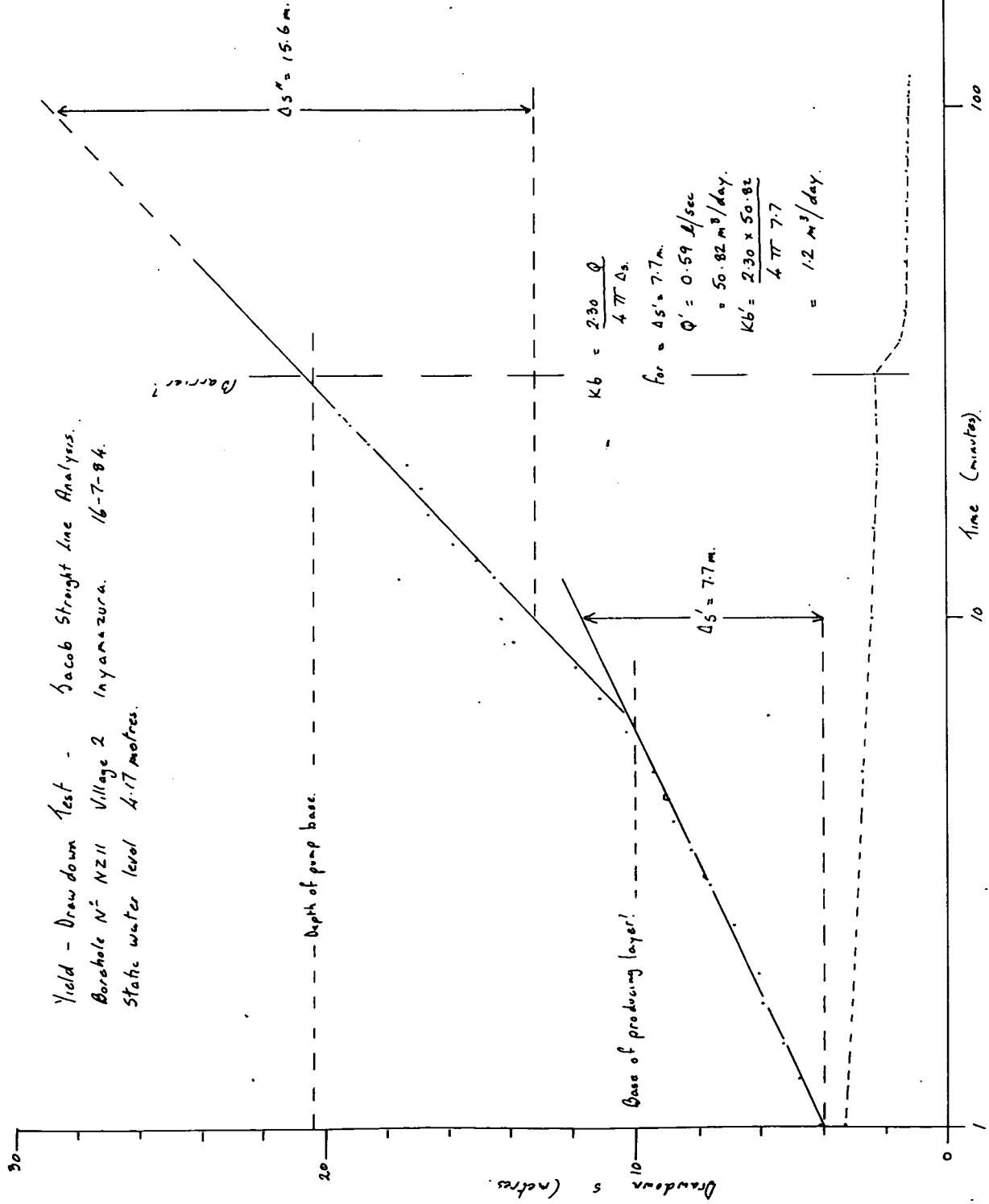
Yield — variable.

Time since pump stopped (mins)	Water level (metres)	<del>Residual</del> draw-down (metres)	Recovery (metres)	t/gi.
0-15				481.
0-30				241
0-45				161.
1-00				121
1-05	23-72	19-55		110.1
1-15	23-36	19-19		97
1-30	23-40	19-02		81
1-45	23-00	18-83		69.6
2-00	22-81	18-64		61
2-30	22- <del>49</del> 49	18-32		49.
3	22-18 <del>22-62</del>	18-01		41
3-30	21-88	17-71		35.3
4	21-62	17-45		31
4-30	21-46	17-29		27.7
5	21-45.5	17-28.5		25
5-30	21-45	17-28		22.8
6	21-30	17-13		21
6-30	21-10	16-93		19.5
7	20-99	16-72		18.1



Recovery Test B/H N <sup>2</sup> N2 11 16-7-84 (cont'd)				
Time since pump stopped (mins)	Water level (metres)	Residual Drawdown (metres)	Recovery (metres)	g/t
8	20-60	16-43		16
9	19-85	15-68		14.3
10	19-13	14-96		13
12	18-20	14-03		11
14	17-72	13-55		9.6
16	17-30	13-13		8.5
18	16-54	12-37		7.7
20	-	-		
22	-	-		
24	-	-		
26	14-20	10-03		5.6
27	14-10	9-93		5.4
28	13-90	9-73		5.3
30	13-53	9-36		5.0
35	12-74	8-57		4.4
40	12-01	7-84		4.0
45	11-32	7-15		3.7
50	10-89	6-72		3.4
55	10-48	6-31		3.2
60	10-14	5-97		3.0
65	9-81	5-64		2.8
8-00 Am (17/7/84)	4-60	0-43		

Yield - Draw down Test - Jacob Straight Line Analysis.  
 Borehole N° N211 Village 2 Inyamazura. 16-7-84.  
 Static water level 4.17 metres.



$$Kb = \frac{230}{4\pi \Delta s}$$

for  $\Delta S'' = 15.6 \text{ m}$

$$Q' = 0.267 \text{ L/sec}$$

$$= 23.0 \text{ m}^3/\text{day}$$

$$Kb = \frac{230}{4\pi \cdot 15.6}$$

$$= 0.270 \text{ m}^3/\text{day}$$

$$Kb = \frac{230}{4\pi \Delta s}$$

for  $\Delta S' = 7.7 \text{ m}$

$$Q' = 0.59 \text{ L/sec}$$

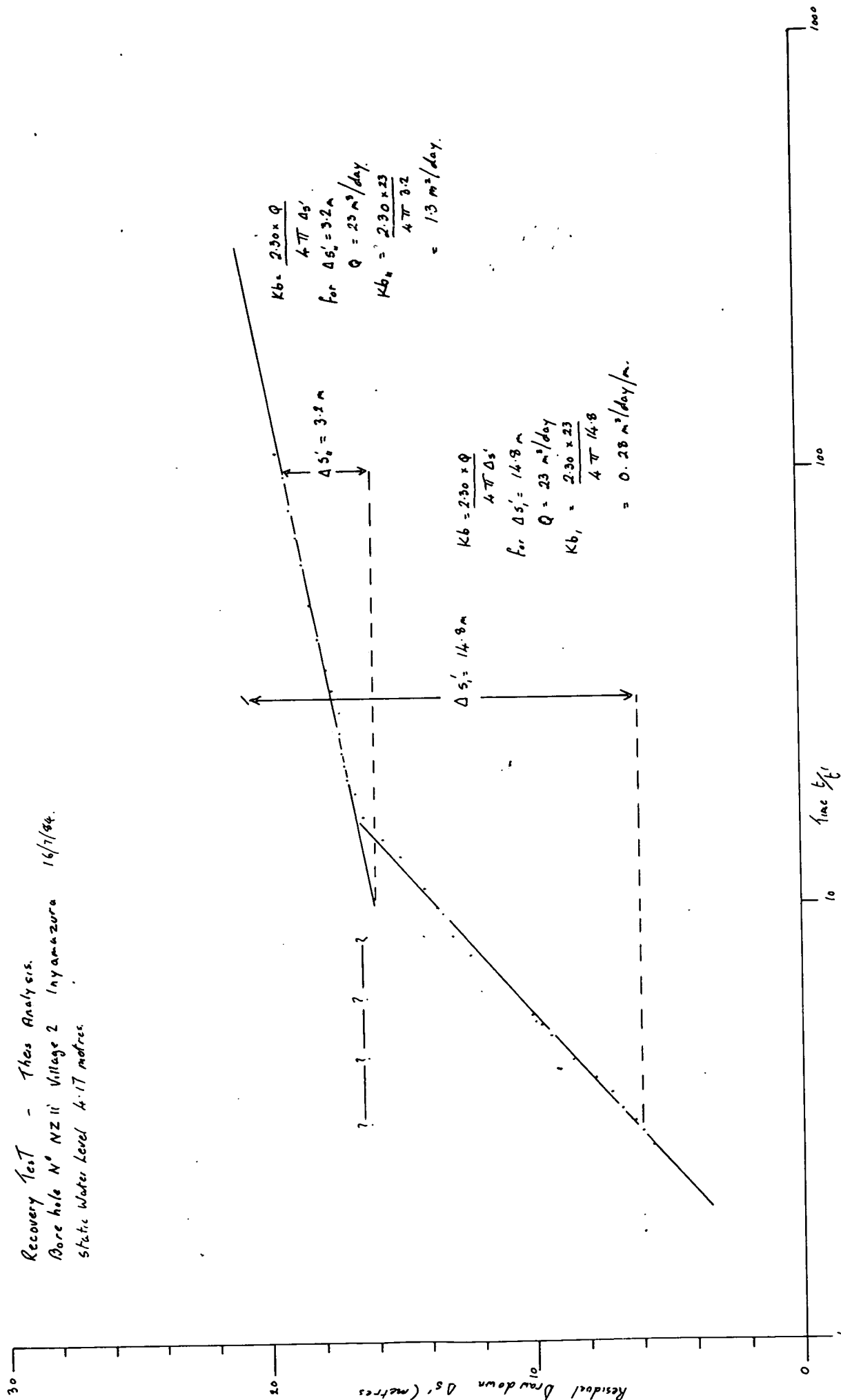
$$= 50.82 \text{ m}^3/\text{day}$$

$$Kb' = \frac{230 \times 50.82}{4\pi \cdot 7.7}$$

$$= 12 \text{ m}^3/\text{day}$$

Yield  
0.5 (l/mes/sec)

Recovery Test - Thes Analysis.  
 Bore hole N° NZ ii Village 2 Inyamazura 16/7/84.  
 Static Water Level 4.17 metres



# Bail Test.

Borchole N° NZ 11 B Village N°2 Nyamazura 31-7-84

REST WATER LEVEL. 6-20 metres.

Capacity of bailer 37 litres.

N° of bails. 21.

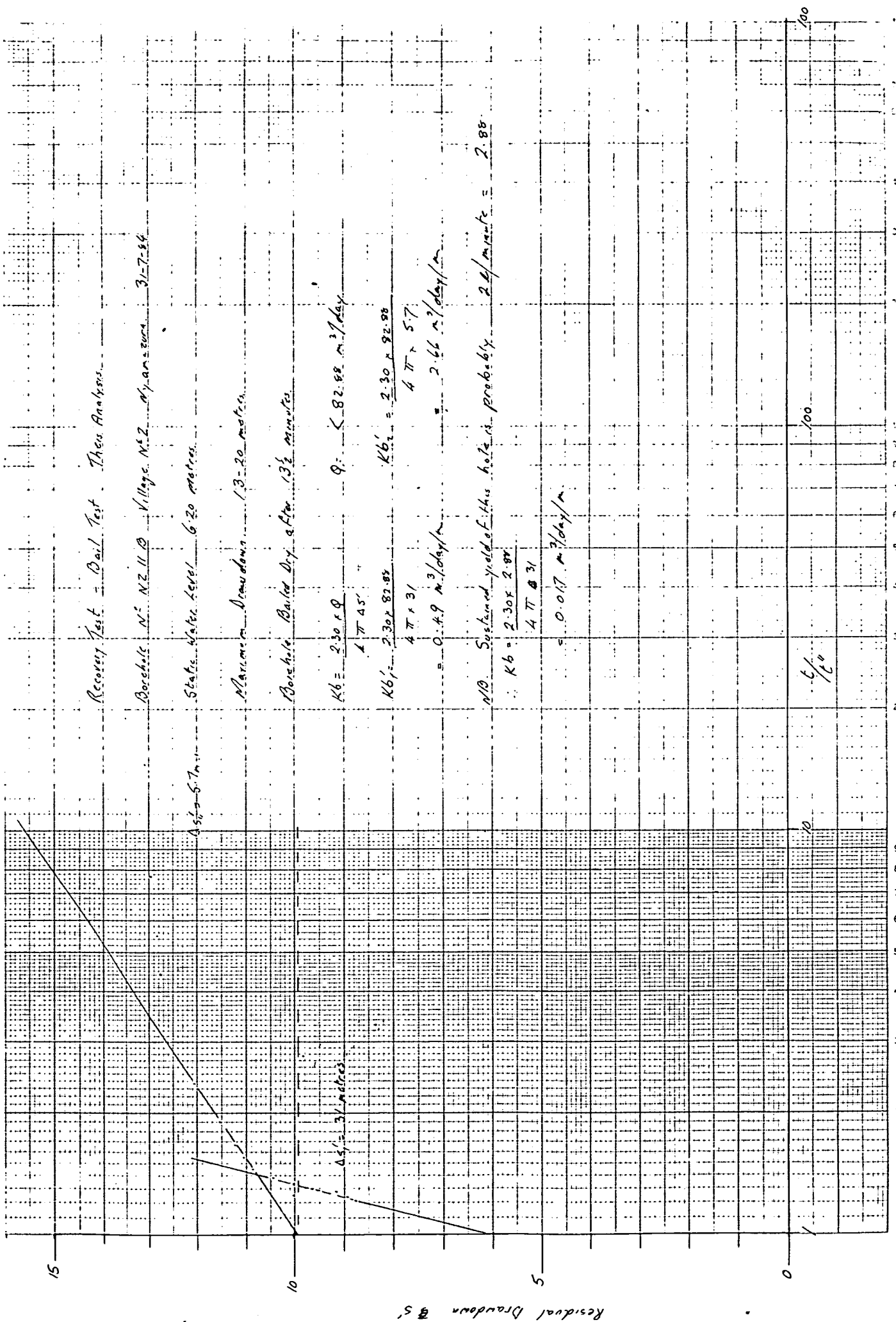
Time taken. 13 mins 30 secs.

Draw down. 13-20 metres.

Amount of water bailed. 777 litres.

Yield 0.96 l/sec. 82.88 m<sup>3</sup>/day - NB well bailed dry after 13½ minutes!

Time after bailing stopped (mins)	Water level (metres)	Residual Drawdown. (metres)	Recovery (metres)	Specific capacity - less than 6.28 m <sup>3</sup> /day/metre of drawdown; $\frac{t}{t'}$
1	19-28	13-0.8	0-12	14.50
2	19-14	12-94	0-26	7.75
3	19-03	12-83	0-37	5.5
4	18-91	12-77	0-43	4.38
5	18-79	12-59	0-61	3.7
10	18-26	12-06	1-14	2.35
15	17-73	11-53	1-67	1.9
20	17-41	11-21	1-99	1.675
25	17-27	11-07	2-13	1.54
30	17-07	10-87	2-33	1.45
35	16-65	10-45	2-75	1.39
40	16-20	10-00	3-20	1.34
45	15-85	9-65	3-55	1.30
50	15-48	9-28	3-92	1.27
55	15-15	8-95	4-25	1.25
60	14-99	8-79	4-41	1.225



Recovery Test = Bail Test. Then Analysis.

Borehole N° N2 11 B Village N°2 Myanmar 3-7-84

ΔS' = 5.7m Static Water Level 6.20 metres

Maximum Drawdown 13.20 metres

Borehole Bailed Dry after 13½ minutes

$$Kb = \frac{2.30 \times Q}{4 \pi \Delta S'} \quad Q = 82.88 \text{ m}^3/\text{day}$$

$$Kb' = \frac{2.30 \times 82.88}{4 \pi \times 31} = 0.49 \text{ m/day/m}$$

$$Kb' = \frac{2.30 \times 82.88}{4 \pi \times 57} = 2.66 \text{ m}^2/\text{day/m}$$

N.B. Sustained yield of this hole is probably 2.6 m³/minute = 2.88

$$Kb = \frac{2.30 \times 2.88}{4 \pi \times 31}$$

$$= 0.017 \text{ m}^3/\text{day/m}$$

t/c

100

100

# Constant Yield Pumping Test.

Bore hole N° NZ 12 A Village N° 10 NYAMAZURA.

Date 17-7-84.

Time test started 15-30 hrs.

Pump cylinder depth 30 metres with 1½" pipe with foot valve to 40 metres.

Ref point — at ground level.

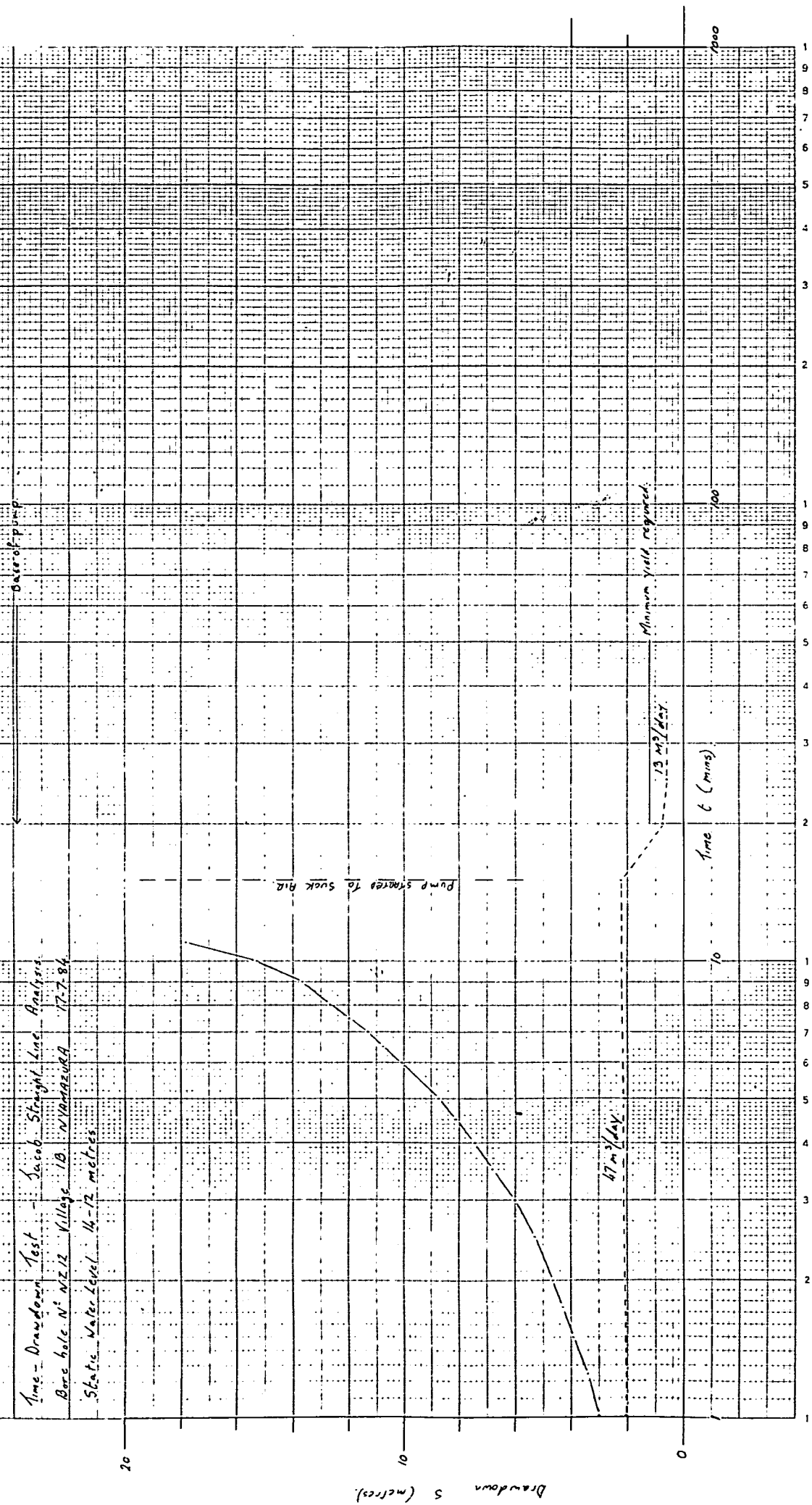
Pump used:- Dando operated single action reciprocating pump.

Time	SWRL (metres)	Time	SWRL	Time	SWRL
15-14	14-04	<del>14-04</del> 13-25	14-12	13-55	14-12
15-29	14-12	13-35	14-12		
13-20	14-13	13-45	14-12		

Time (mins)	Water level (metres)	Drawdown (metres)	Yield (Secs/20 cl)	Temp. (°C)	Conductivity μ S	pH.
0-15	15-77	1-65	33-7	23.4	310	8-25
0-30	16-12	2-00				
0-45	16-72	2-60				
1-00	17-13	3-01				
1-15	17-53	3-41				
1-30	18-06	3-94				
1-45	18-40	4-28				
2-00	18-73	4-61				
2-30	19-45	5-33				
3-00	20-13	6-01				
3-30	20-94	6-32				
4-00	21-55	7-43				
4-30	22-27	8-15				
5	22-90	8-78	37.5	23.4	310	7.85
6	24-20	10-08				

Constant Yield Pumping Test. Borehole NZ 12. Village 1B. 17-7-84 (cont'd)

[illegible]





# Bail Test.

Borehole N° NZ 12B. Village N° 1B Nyamazura. 9-8-84.

Rest water level. 6-53 metres.

Capacity of bailer. 37 litres

N° of bails. 51.

Time taken. 30 minutes.

Draw down. 4-47 metres.

Amount of water bailed. 1.887 m<sup>3</sup>.

Yield. 1.05 l/sec. 90.58 - m<sup>3</sup>/day

Specific capacity 20.26 m<sup>3</sup>/day / metre of drawdown.

Time after bailing stopped. (mins.)	Water level. (metres)	Residual Drawdown. (metres)	Recovery (metres)	$\frac{t}{t'}$
1	10-98	4-45	0-02	31
2	10-96	4-43	0-04	16
3	9-94	3-41	1-06	11
4	9-37	2-84	1-63	8.5
5	9-12	2-69	1-78	7
10	8-27	1-74	2-73	4
15	7-98	1-45	3-02	3
20	7-80	1-27	3-20	2.5
25	7-67	1-14	3-33	2.2
30	7-56	1-03	3-44	2
35	7-46	0-93	3-54	1.86
40	7-35	0-82	3-65	1.75
45	7-11	0-58	3-89	1.67
50	6-82	0-29	4-18	1.60
55	6-72	0-19	4-28	1.55
60	6-68	0-15	4-32	1.50

Bad Test - Recovery Data Theys Analysis

Borchiole N° 13 Village N° 13 N.Y. 9-8-84

Rest water level 6.53 metres

Maximum Drawdown 4.4 months

90.58 sec / day

Duration of test: 30 minutes.

$$k' = 2.3 \times 10^{-58}$$

1	4	7	9
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$$= 5.72 \text{ m}^3/\text{day}/\text{metric}$$

$$\Delta s' = 2.9 \text{ metres}$$

Residual Drawdown S'

1000

100

$$t/t''$$

10

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100	101	102	103	104	105	106	107	108	109	110	111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139	140	141	142	143	144	145	146	147	148	149	150	151	152	153	154	155	156	157	158	159	160	161	162	163	164	165	166	167	168	169	170	171	172	173	174	175	176	177	178	179	180	181	182	183	184	185	186	187	188	189	190	191	192	193	194	195	196	197	198	199	200	201	202	203	204	205	206	207	208	209	210	211	212	213	214	215	216	217	218	219	220	221	222	223	224	225	226	227	228	229	230	231	232	233	234	235	236	237	238	239	240	241	242	243	244	245	246	247	248	249	250	251	252	253	254	255	256	257	258	259	260	261	262	263	264	265	266	267	268	269	270	271	272	273	274	275	276	277	278	279	280	281	282	283	284	285	286	287	288	289	290	291	292	293	294	295	296	297	298	299	300	301	302	303	304	305	306	307	308	309	310	311	312	313	314	315	316	317	318	319	320	321	322	323	324	325	326	327	328	329	330	331	332	333	334	335	336	337	338	339	340	341	342	343	344	345	346	347	348	349	350	351	352	353	354	355	356	357	358	359	360	361	362	363	364	365	366	367	368	369	370	371	372	373	374	375	376	377	378	379	380	381	382	383	384	385	386	387	388	389	390	391	392	393	394	395	396	397	398	399	400	401	402	403	404	405	406	407	408	409	410	411	412	413	414	415	416	417	418	419	420	421	422	423	424	425	426	427	428	429	430	431	432	433	434	435	436	437	438	439	440	441	442	443	444	445	446	447	448	449	450	451	452	453	454	455	456	457	458	459	460	461	462	463	464	465	466
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